

Induced Seismicity Workshop
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From Hazard Assessment to Hazard Management

The Case of Mining-Induced Seismicity

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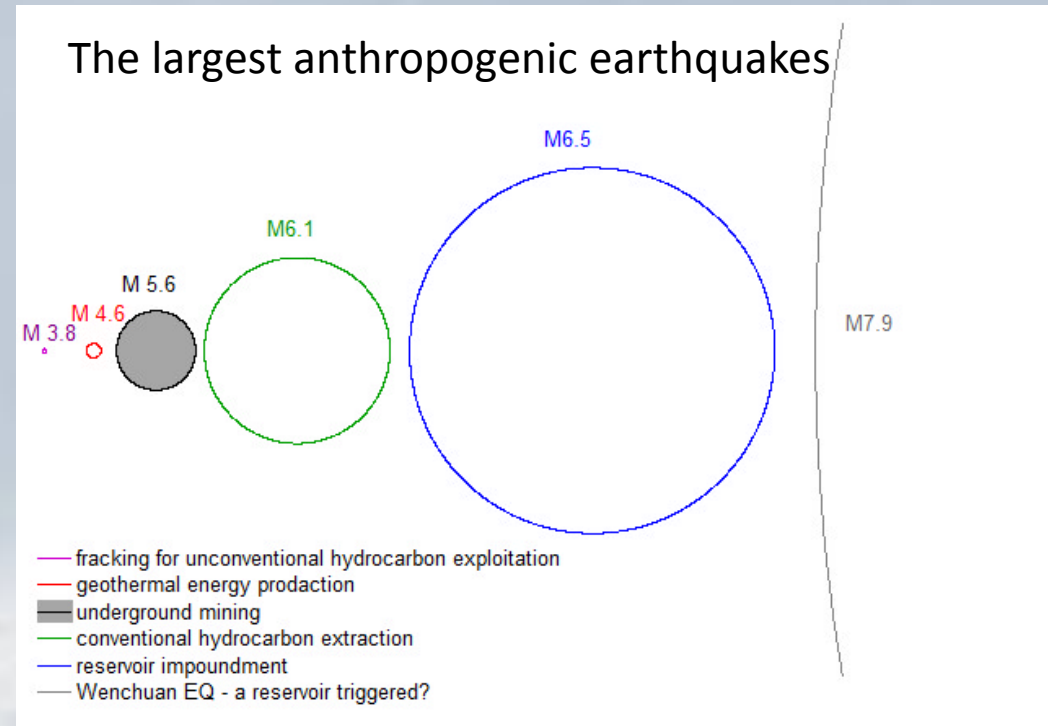
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SEISMOLOGY AND PHYSICS OF THE EARTH'S INTERIOR, LITHOSPHERE RESEARCH, GEOMAGNETISM, PHYSICS OF ATMOSPHERE
HYDROLOGY AND HYDRODYNAMICS, POLAR RESEARCH, CENTRAL GEOPHYSICAL OBSERVATORY AT BELSK

MINING-INDUCED SEISMICITY

The first chronicled rockburst in Derbyshire, England, 1738

The strongest event M5.6 Ernst Thaelmann Potash Mine, Volkershausen, Germany, 13/03/1989



Geographical Distribution:

Austria, Czech Rep. Finland, France, Germany, Poland, Russia, Spain, Sweden, UK, Ukraine

Canada, USA, Chile, Rep. of South Africa

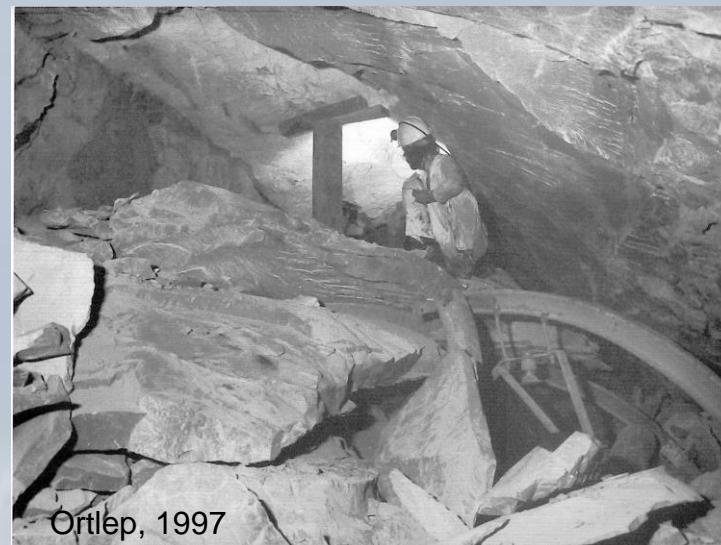
China, India, Japan, Australia



Stronger Mining Induced Seismic (MIS) Events Cause Material Loss, Injuries, Sometimes Fatalities



Underground





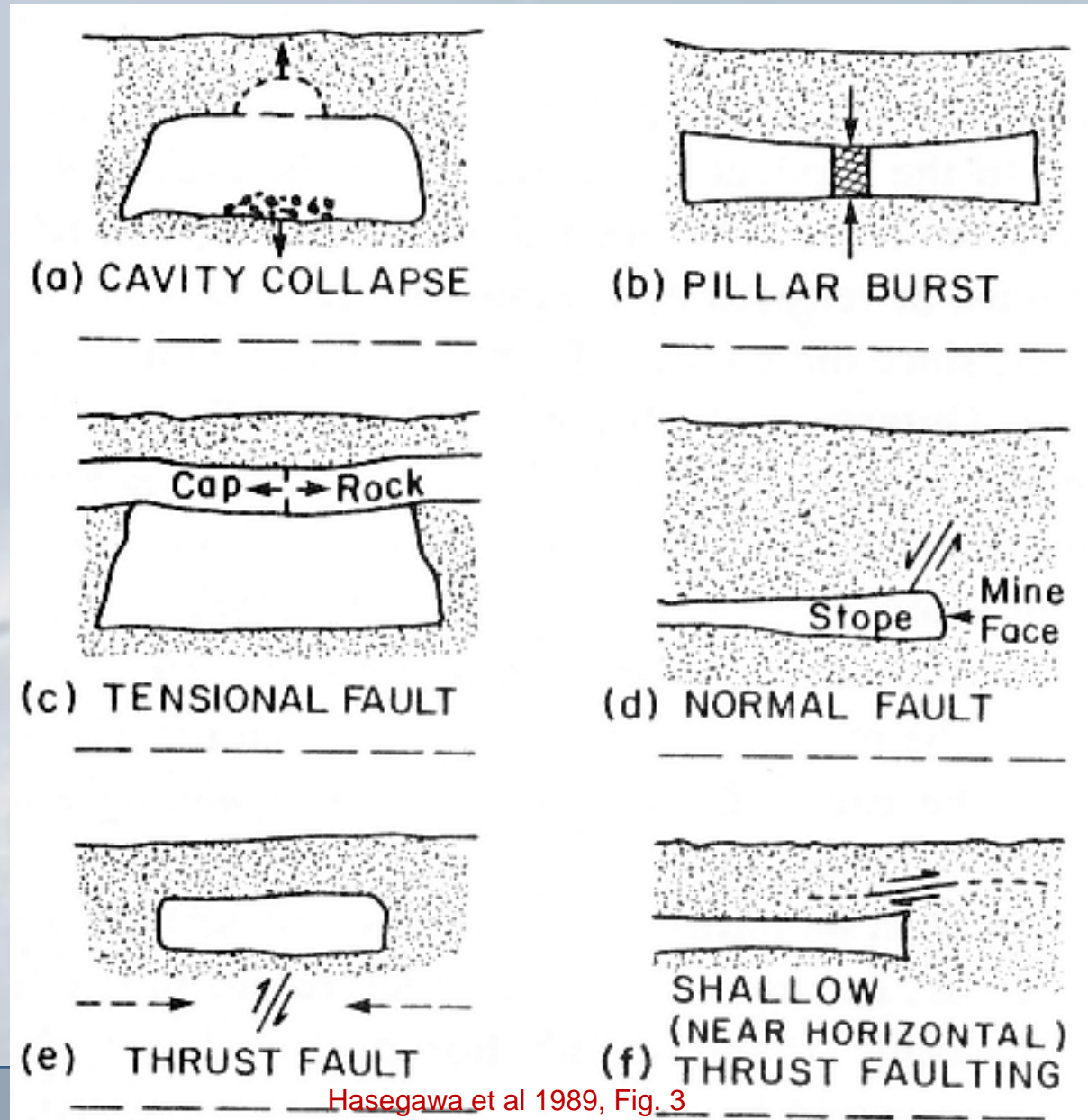
Durrheim 2010

Ground effects



Mining Seismicity is Induced

Strains in the rockmass that lead to seismic events are primarily due to the stress field changes caused by mining openings.



Hasegawa et al 1989, Fig. 3



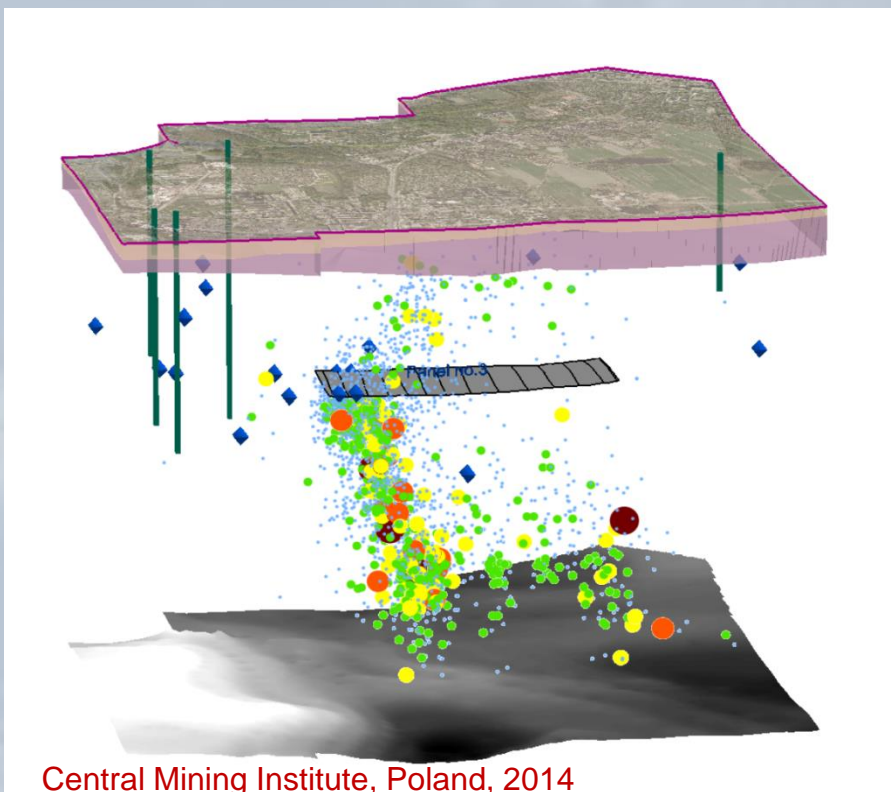
Internal Division of MIS Events

INDUCED: linked directly to mining operations. Cluster around mining stopes and follow mining works.

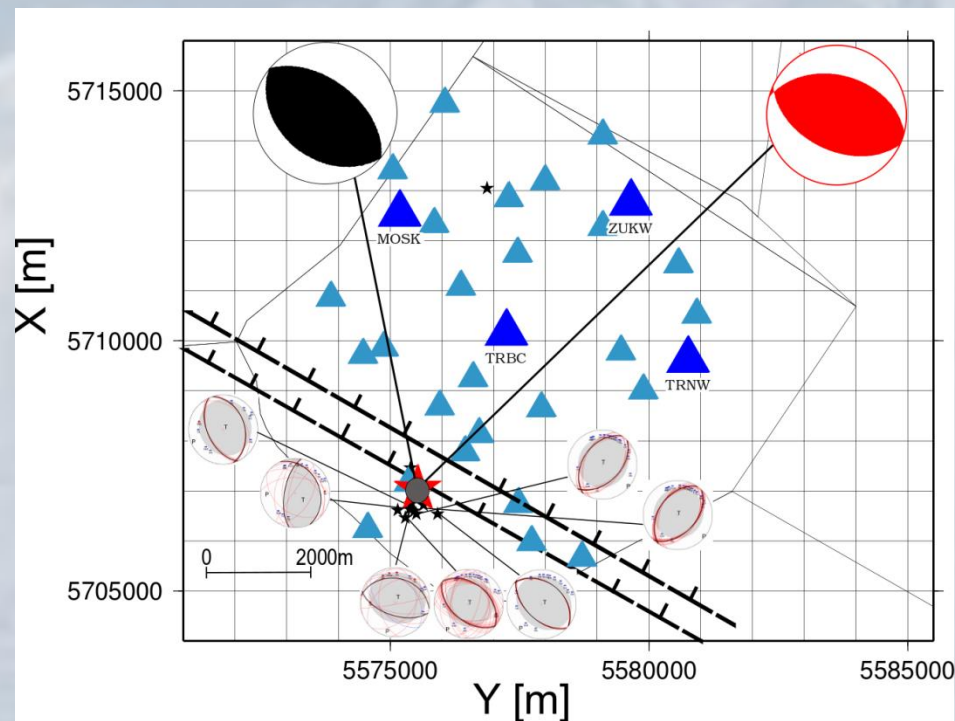
&

TRIGGERED: result from regional stress redistribution caused by mining. Occur farther from mining works in geologically disturbed areas.

Johnston and Einstein, 1990



Central Mining Institute, Poland, 2014

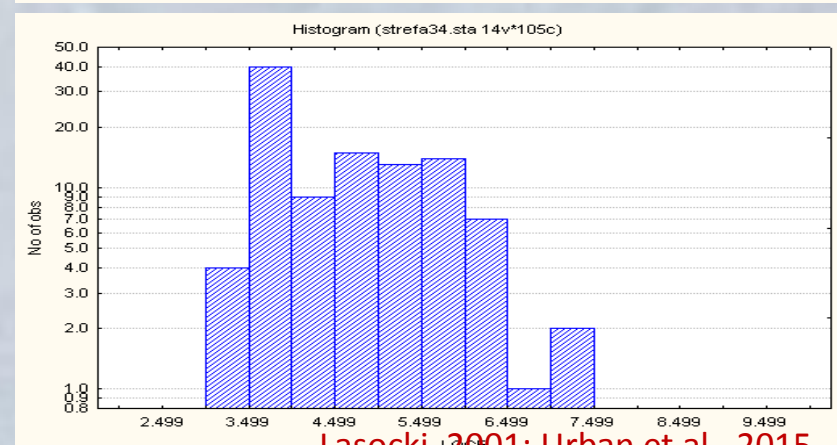
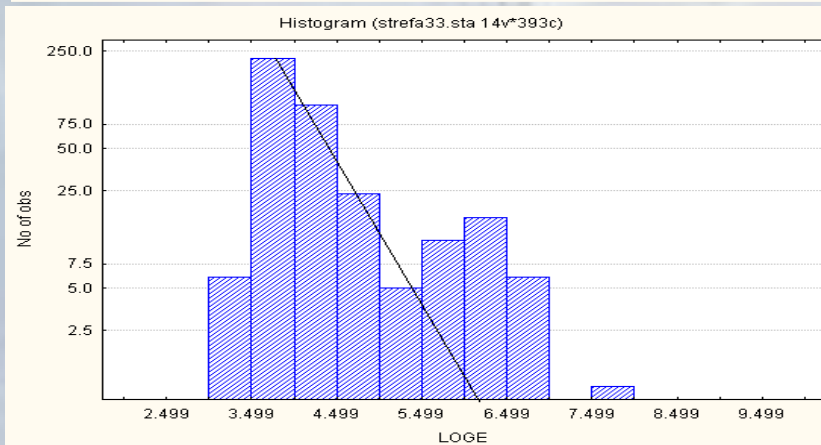
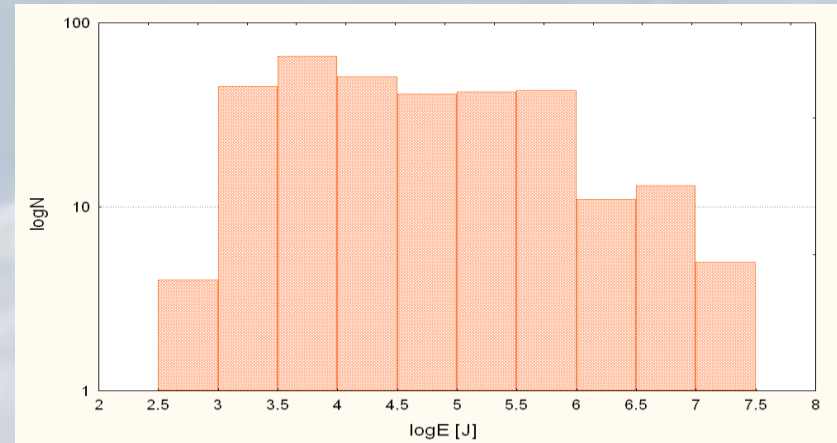
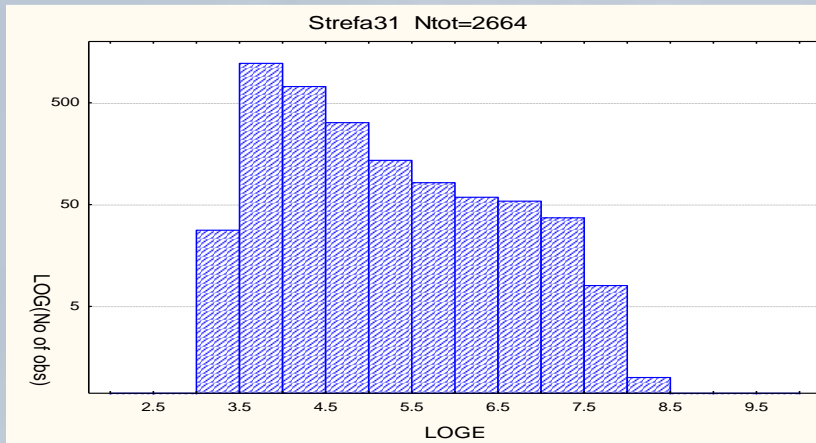


Lizurek, et al., 2015



MIS Population is Mixed f At Least Two Components: The Directly Linked To Mining And The Triggered By Mining

⇒ Magnitude distributions are complex and often multimodal. The Gutenberg-Richter distribution model is not relevant (*the feature of all kinds of AS*)



Lasocki, 2001; Urban et al., 2015



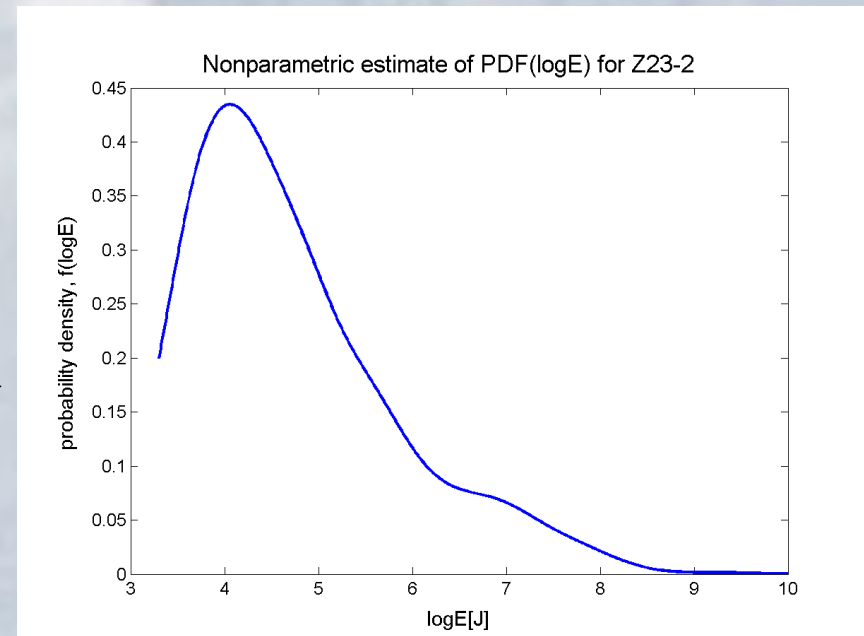
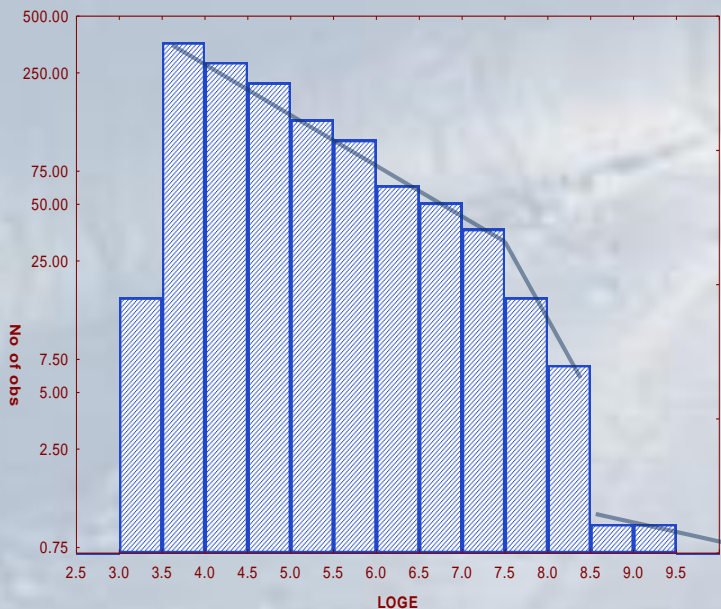
⇒ A model free approach is used to estimate MIS magnitude distributions, based on non-parametric kernel estimators

Kijko et al. 2001; Lasocki and Orlecka-Sikora, 2008

$$\hat{f}_m^a(m) = \frac{(\sqrt{2\pi})^{-1} \sum_{i=1}^n \frac{1}{\alpha_i h} \exp\left[-0.5\left(\frac{m-m_i}{\alpha_i h}\right)^2\right]}{\sum_{i=1}^n \left[\Phi\left(\frac{m_{\max} - m_i}{\alpha_i h}\right) - \Phi\left(\frac{m_{\min} - m_i}{\alpha_i h}\right) \right]}$$

$$\hat{F}_m^a(m) = \frac{\sum_{i=1}^n \left[\Phi\left(\frac{m-m_i}{\alpha_i h}\right) - \Phi\left(\frac{m_{\min} - m_i}{\alpha_i h}\right) \right]}{\sum_{i=1}^n \left[\Phi\left(\frac{m_{\max} - m_i}{\alpha_i h}\right) - \Phi\left(\frac{m_{\min} - m_i}{\alpha_i h}\right) \right]}$$

$$\hat{m}_{\max} = m_{\max}^{obs} + \int_{m_{\min}}^{\hat{m}_{\max}} \left[\hat{F}_m^a(m) \right]^n dm$$

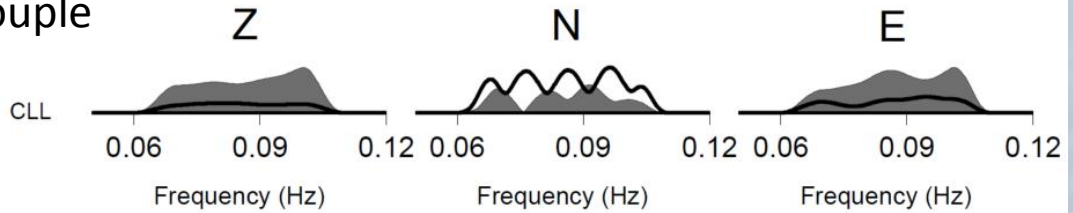
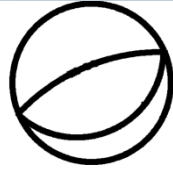


MIS Events have often extended sources with significant non-DC components *(the feature of all kinds of AS)*

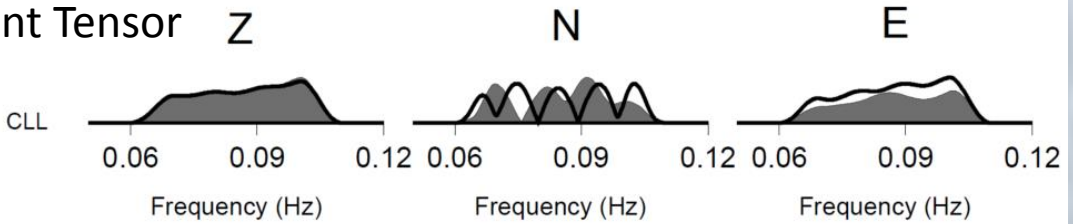
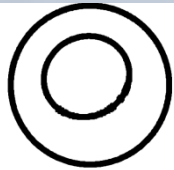
Mw3.8 19/03/2013
19 miners stacked

(Rudziński et al, 2015)

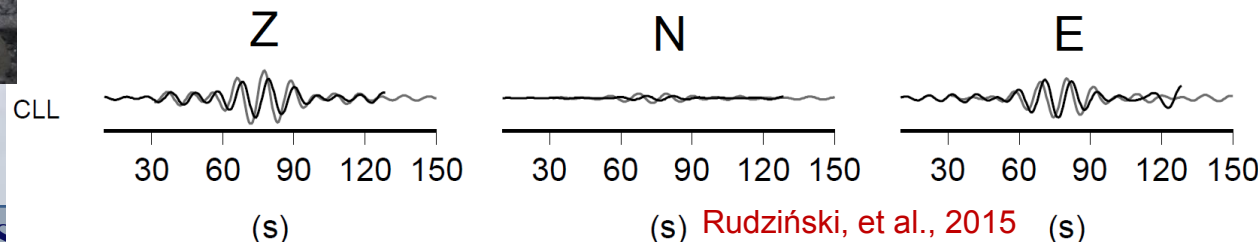
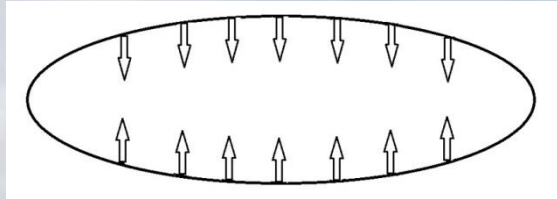
Double-Couple



Full Moment Tensor



Tabular Cavity collapse model



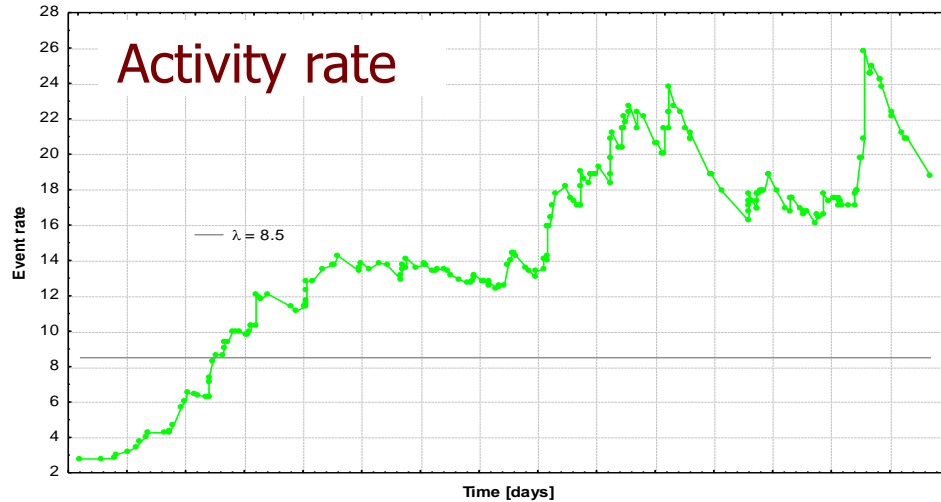
(s) Rudziński, et al., 2015 (s)



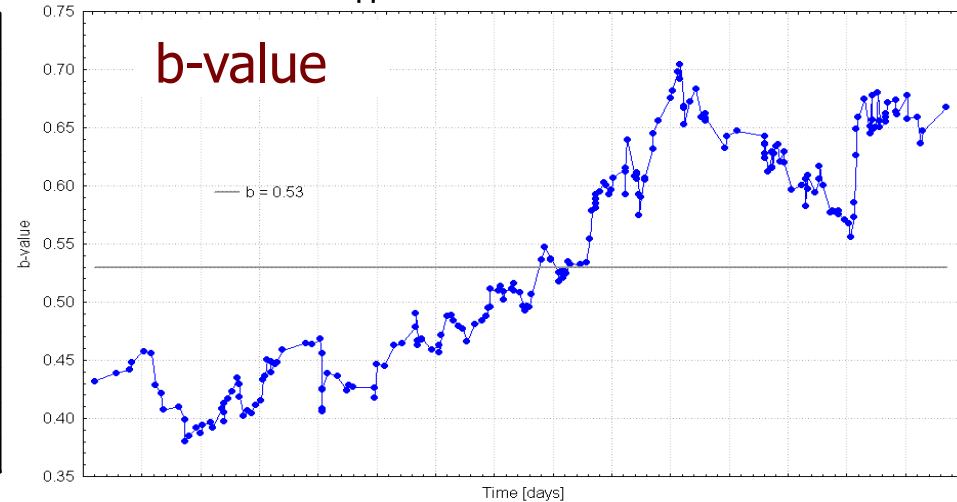
MIS is controlled primarily by time varying mining works

⇒ Within individual active zones the activity rate and the event size distribution change in time

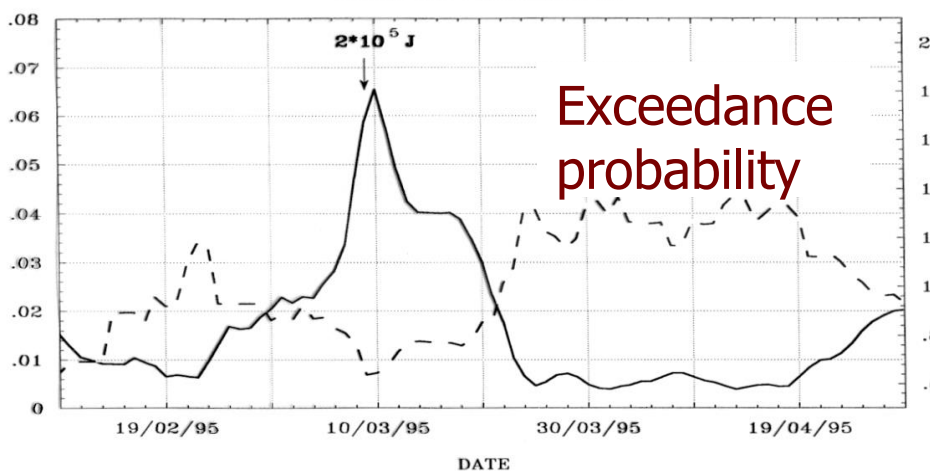
G24-4 22.02.2003-31.10.2005



Rudna Copper Mine G24-4 22.02.2003-31.10.2005



WUJEK MINE LONGWALL 5A



Rudna Copper Mine G24-4 22.02.2003-31.10.2005

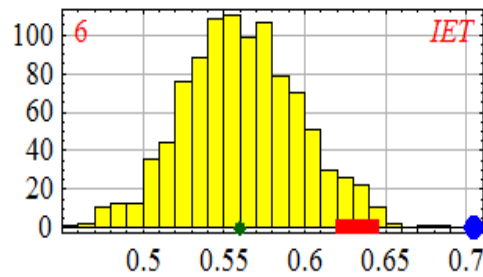


Lasocki, 2009

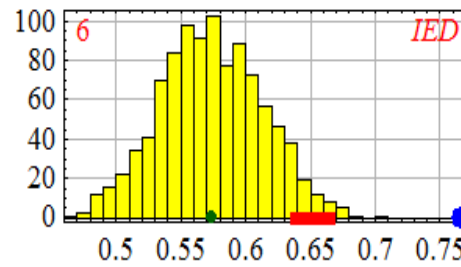


Events are interrelated in a short as well as in a long time scale.

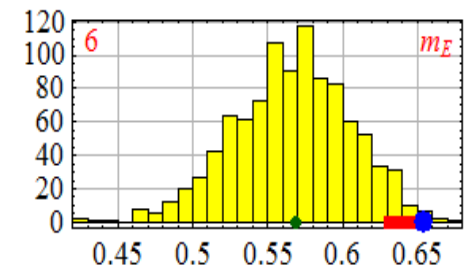
Interevent Time



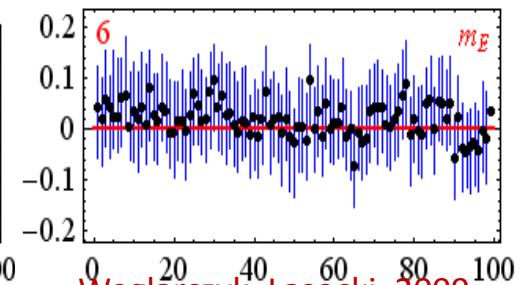
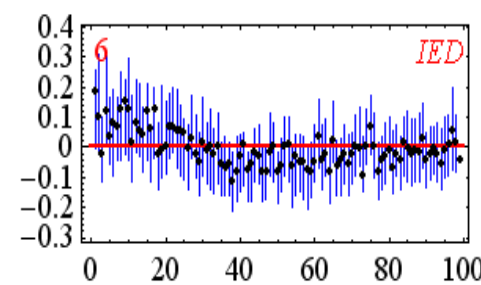
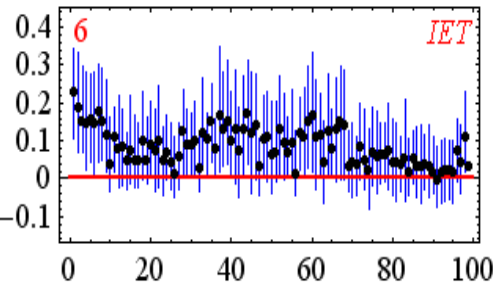
Interevent Distance



Magnitude



Long Memory:
Hurst R/S Analysis



Short Memory:
ACC Analysis

Węglarczyk, Lasocki, 2009



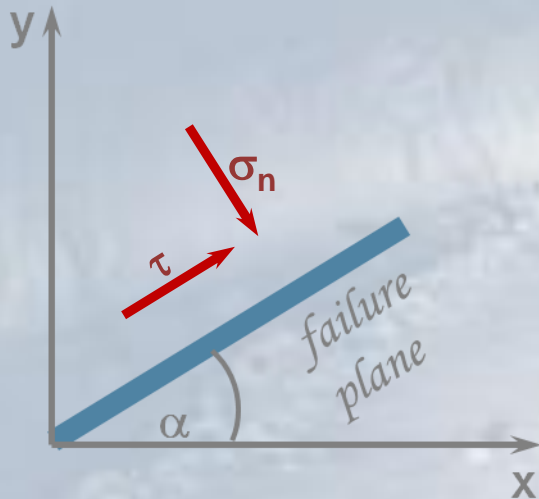
Static stress change due to coseismic displacement plays an important role for subsequent event generation

(the feature of all kinds of AS)

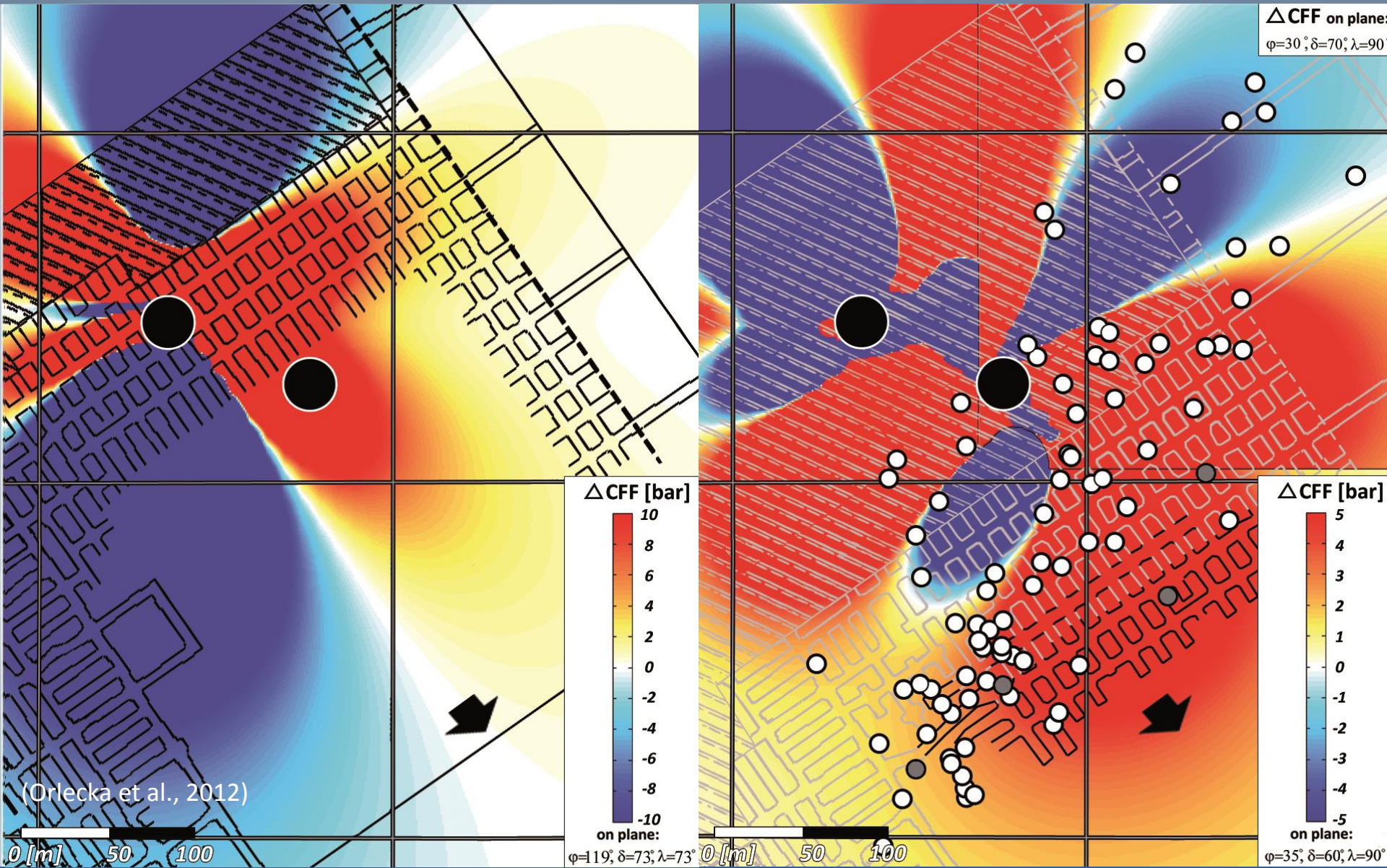
Coulomb Failure Criterion:

$$\Delta CFF = \Delta \sigma_f = \Delta \tau - \mu(\Delta \sigma_n - p)$$

- $\Delta \tau$ - the shear stress on failure plane
- $\Delta \sigma_n$ - the normal stress
- p - the pore fluid pressure
- μ - the coefficient of friction



G-1 1/8 section



CONCLUSIONS ON ASSESSMENT OF SEISMIC HAZARD

- ❑ *Due to specific features of MIS the seismic hazard analysis must undergo substantial modifications to be applicable to MIS problems.*
- ❑ *One has to take into account complexity of source mechanisms, transient and time-varying character of the seismic process, complexity of magnitude distribution, interrelations among events.*
- ❑ *The seismic hazard cannot be reliably assessed without considering technological factors conditioning the seismic process.*
- ❑ *Due to the dependence of the seismic process on technological activity the results of hazard analysis are predictions related to a prescribed time period.*
- ❑ *The above conclusions extend onto all kinds of anthropogenic seismicity*

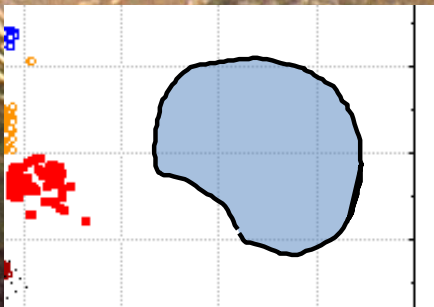


A CASE STUDY OF ASSESSEMENT AND MANAGEMENT OF THE SEISMIC HAZARD DUE TO MIS

(Lasocki et al. 2011; 2012)

Prediction of limiting values of ground motion acceleration components at selected points along the dam of Želazny Most tailings pond for the period 2011/2012-2050

- total area: 12.4km²
- earth dams' length: 14.4km
- final hight of earth dams: up to 100m
- final capacity (planned): 1000 mln. m³



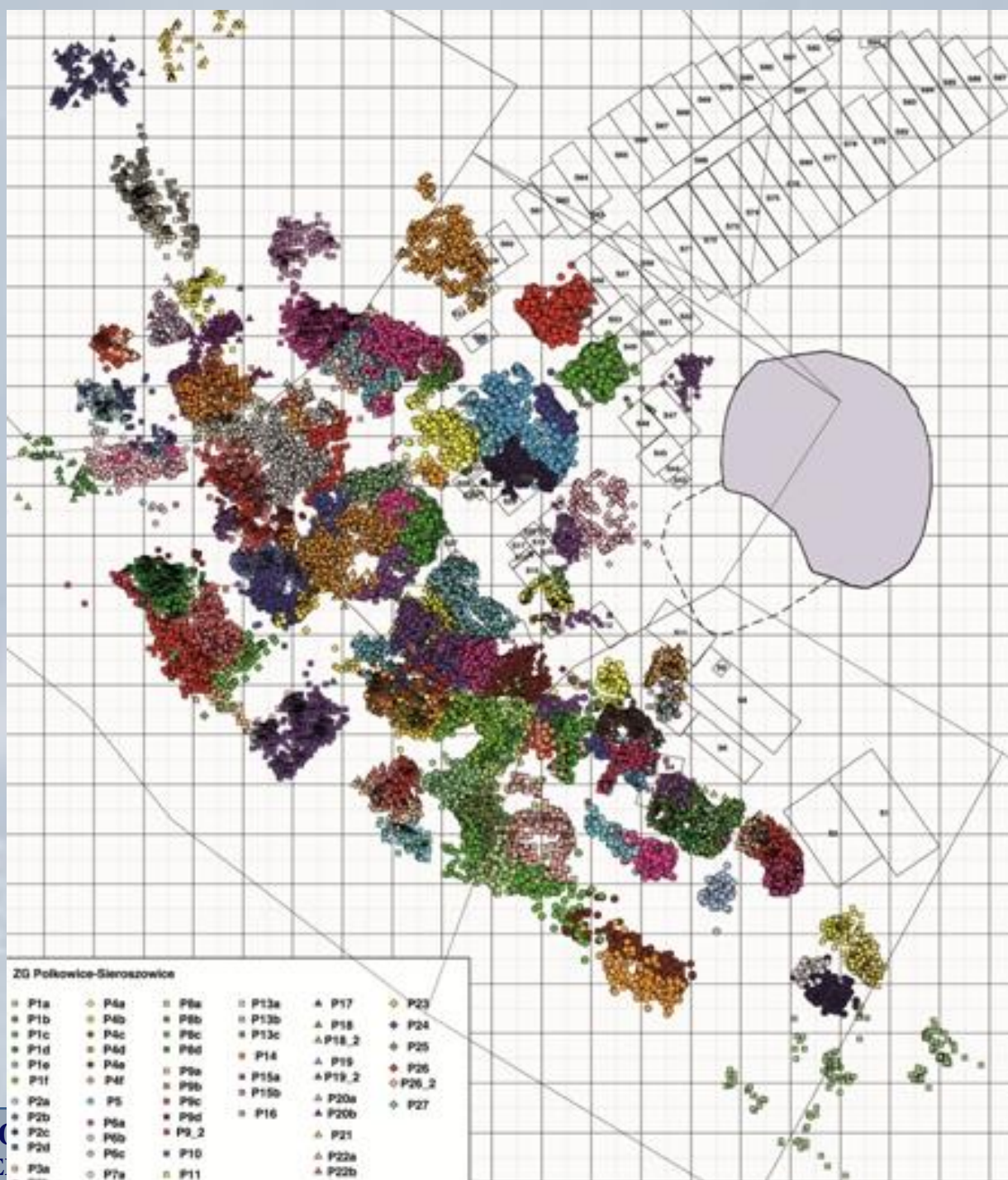
A CASE STUDY OF ASSESSEMENT AND MANAGEMENT OF THE SEISMIC HAZARD DUE TO MIS

Prediction of limiting values of ground motion acceleration components at selected points along the dam of Źelazny Most tailings pond for the period 2011/2012-2050

Assumptions:

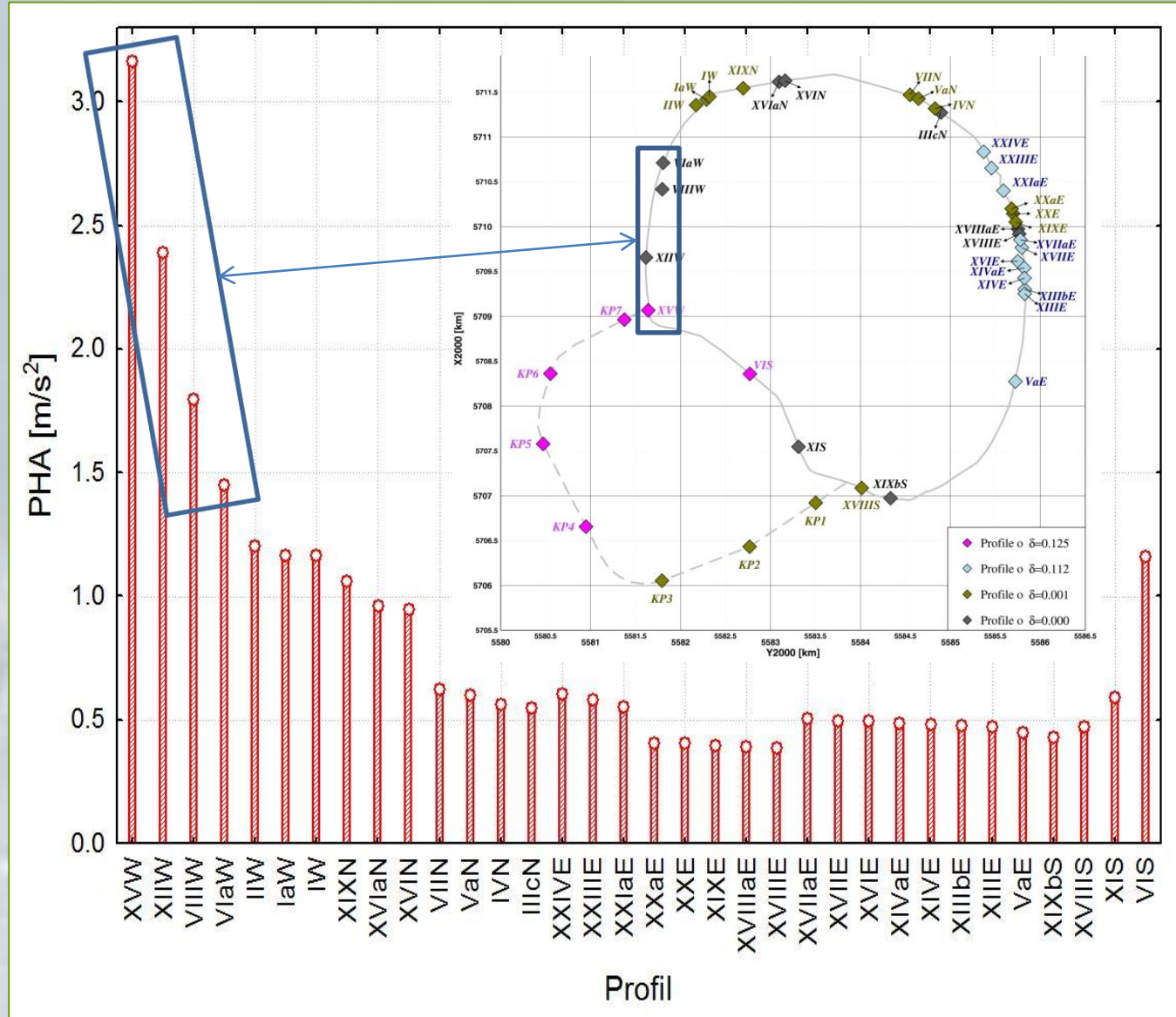
- The limiting value = PGA of exceedance probability 5%.
- The analysis takes into account impacts of mining works planned for the years 2011-2050 within a 5 km wide zone around the protecting pillar of the pond. (84 mining panels).





Limiting PHA predicted for 2011-2050. Exceedance probability = 0.05

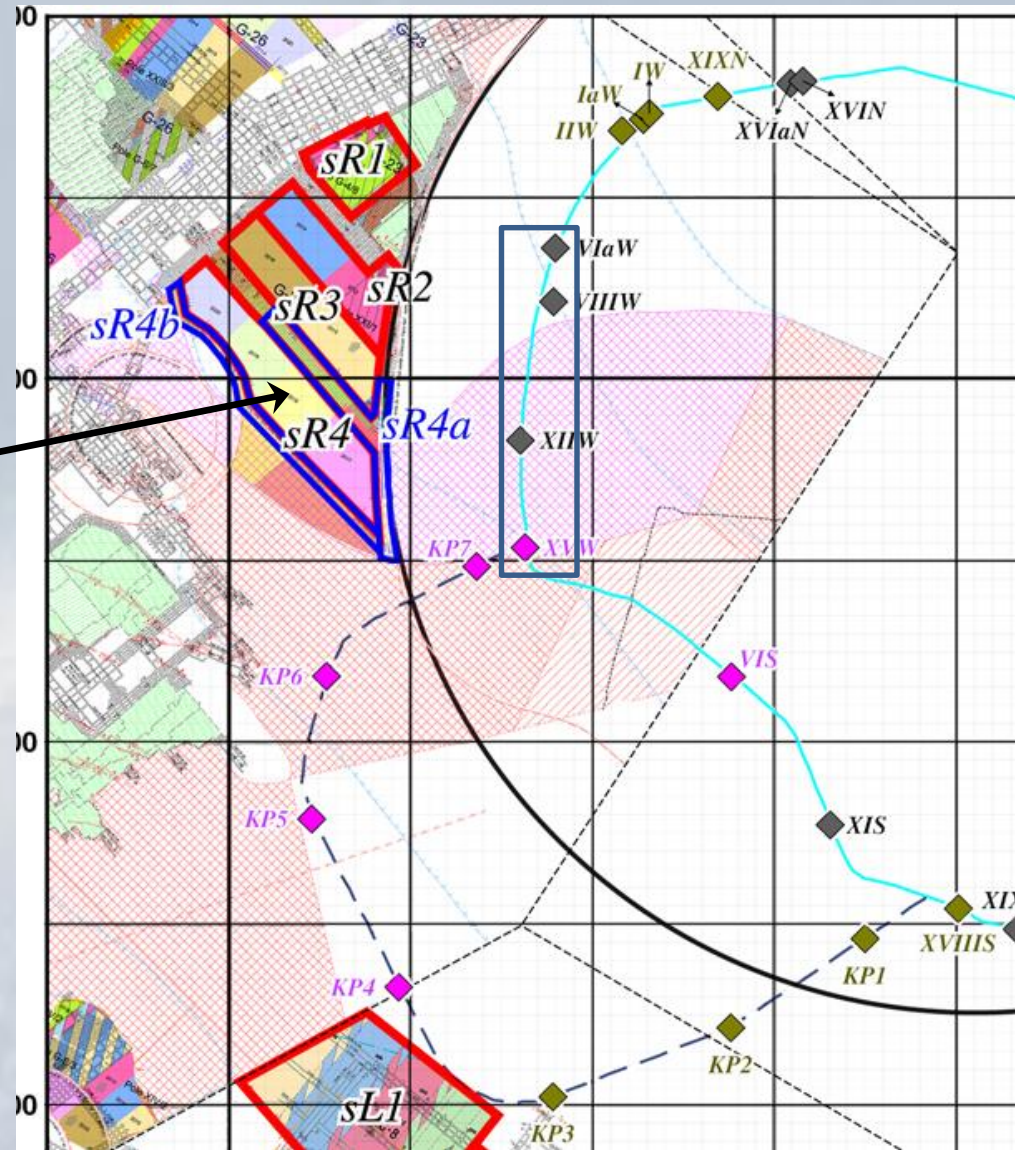
PROFIL	X 2000	Y 2000	PHA [m/s ²]
XVW	5709066	5581643	3.17
XIIW	5709658	5581614	2.39
VIIIW	5710416	5581643	1.79
VlaW	5710712	5581808	1.45
IIW	5711356	5582173	1.20
IaW	5711418	5582290	1.17
IW	5711452	5582322	1.16
XIXN	5711545	5582697	1.06
XVIaN	5711617	5583095	0.96
XVIN	5711627	5583162	0.94
VIIIN	5711469	5584553	0.62
VaN	5711428	5584645	0.60
IVN	5711316	5584830	0.56
IIIcN	5711272	5584895	0.55
XXIVE	5710834	5585370	0.60
XXIIIIE	5710655	5585460	0.58
XXIaE	5710400	5585590	0.55
XXaE	5710200	5585680	0.41
XXE	5710145	5585698	0.40
XIXE	5710053	5585728	0.40
XVIIIaE	5709973	5585754	0.39
XVIIIIE	5709919	5585766	0.39
XVIIaE	5709854	5585779	0.50
XVIIIE	5709766	5585796	0.50
XVIE	5709614	5585748	0.49
XIVaE	5709540	5585820	0.49
XIVE	5709426	5585823	0.48
XIIIbE	5709301	5585826	0.47
XIIIIE	5709253	5585828	0.47
VaE	5708275	5585722	0.45
XIXbS	5706974	5584335	0.43
XVIIIIS	5707088	5584015	0.47
XIS	5707545	5583312	0.59
VIS	5708360	5582770	1.16



Recommendations For The Company Management

In order to decrease seismic hazard to an acceptable level:

1. Exploitation in panels described as sR4 zones should be suspended
2. Exploitation within zones sR1-sR3 should be directed from the border of protecting pillar outwards (towards NW)



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Thank you for attention



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