

Resolution of non-DC components of MTs induced during EGS stimulations and their implications at Utah FORGE

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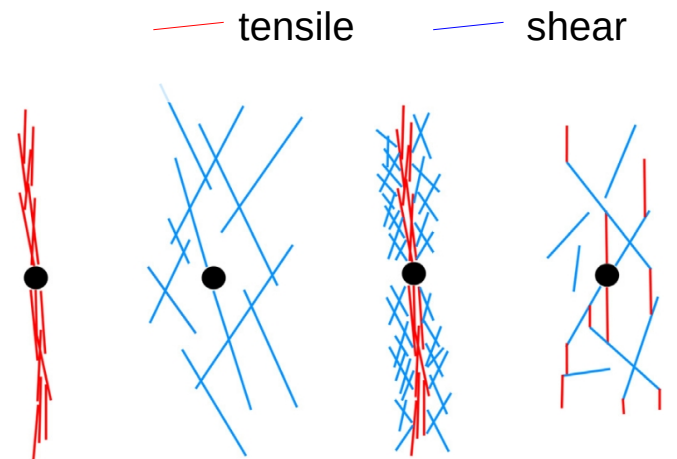
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³ Santa Fe Seismic LLC, Santa Fe, New Mexico, USA

Motivation

Are double-couple (DC) components of microseismic MTs representative for the reservoir hydrofracture geometry?

Can tensile/non-DC components provide insight into permeability of the reservoir?



McClure and Horn (2014)

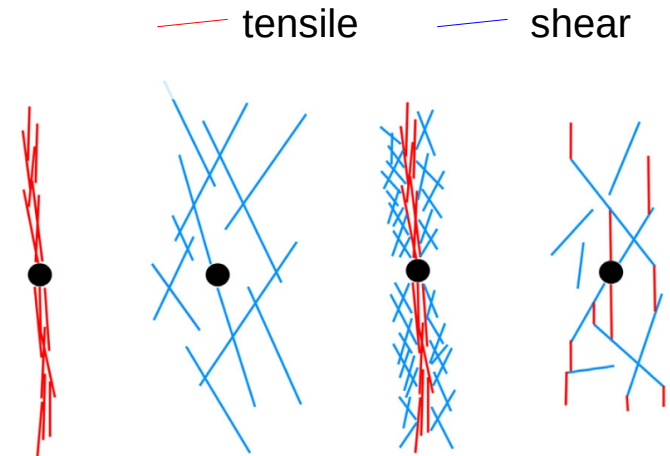
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MT inversions

- velocity model resolution \leftrightarrow dominant frequencies
- simplicity \leftrightarrow complexity
- magnitude \leftrightarrow hypocentral distances



McClure and Horn (2014)

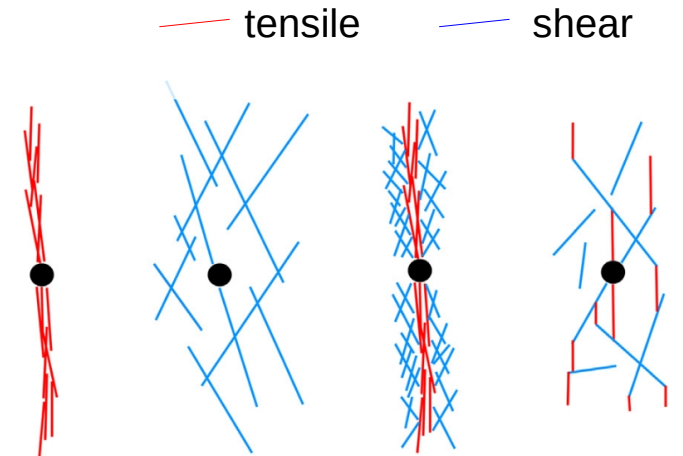
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MT inversions

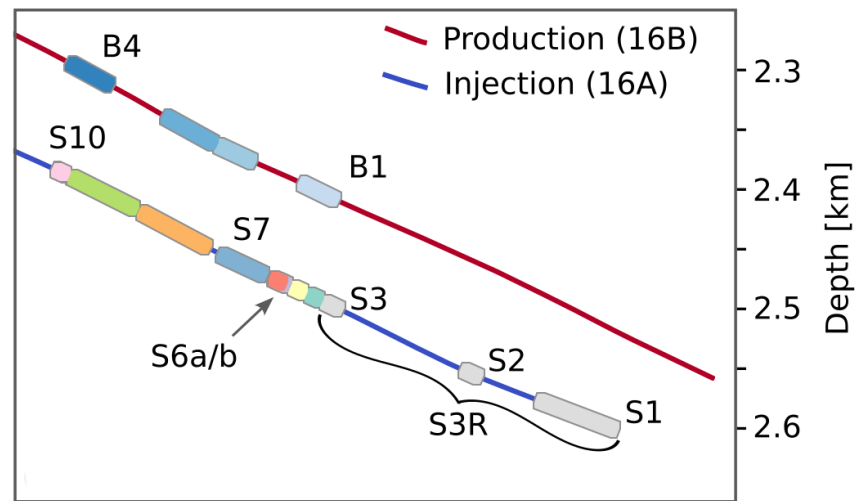
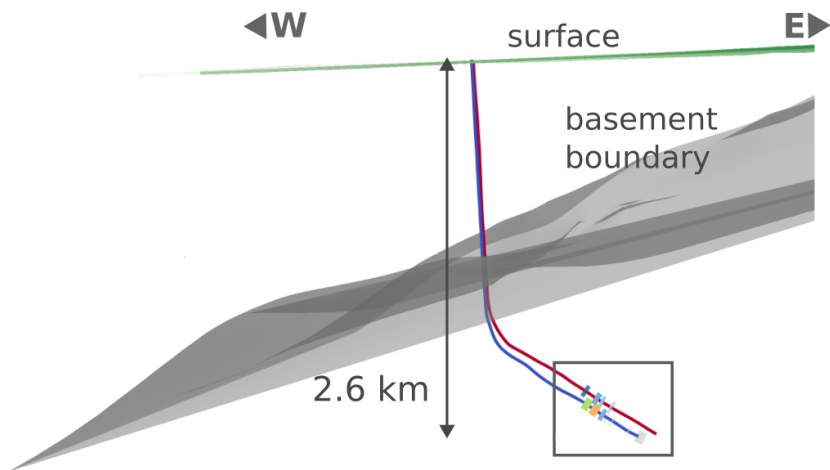
- velocity model resolution \leftrightarrow dominant frequencies
 - simplicity \leftrightarrow complexity
 - magnitude \leftrightarrow hypocentral distances
- at the limits of full-waveform inversion
→ assessing uncertainties and limitations is important



McClure and Horn (2014)

Utah FORGE - Stimulations 2024

Utah Frontier Observatory for Research in Geothermal Energy



2022 Stimulation
16A

2023 Circulation
16A → 16B

2024 Stimulation
16A

2024 Stimulation
16B

S3 S2 S1

April
2022

→ 16B

July
2023

S3R S4 S5 S6a/b S7 S8 S9 S10

April 3 - 7
2024

B1 B2 B3 B4

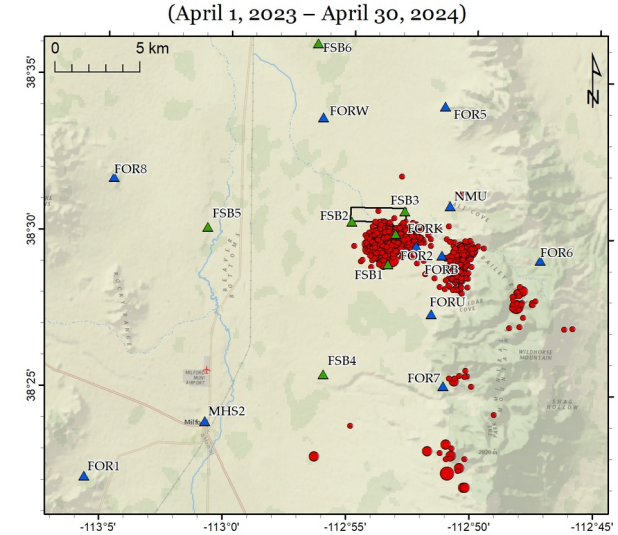
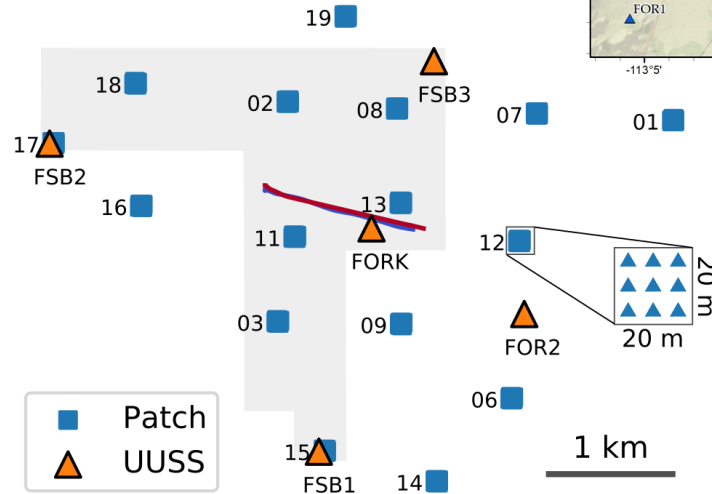
April 11 - 17
2024

Microseismic surface monitoring at Utah FORGE

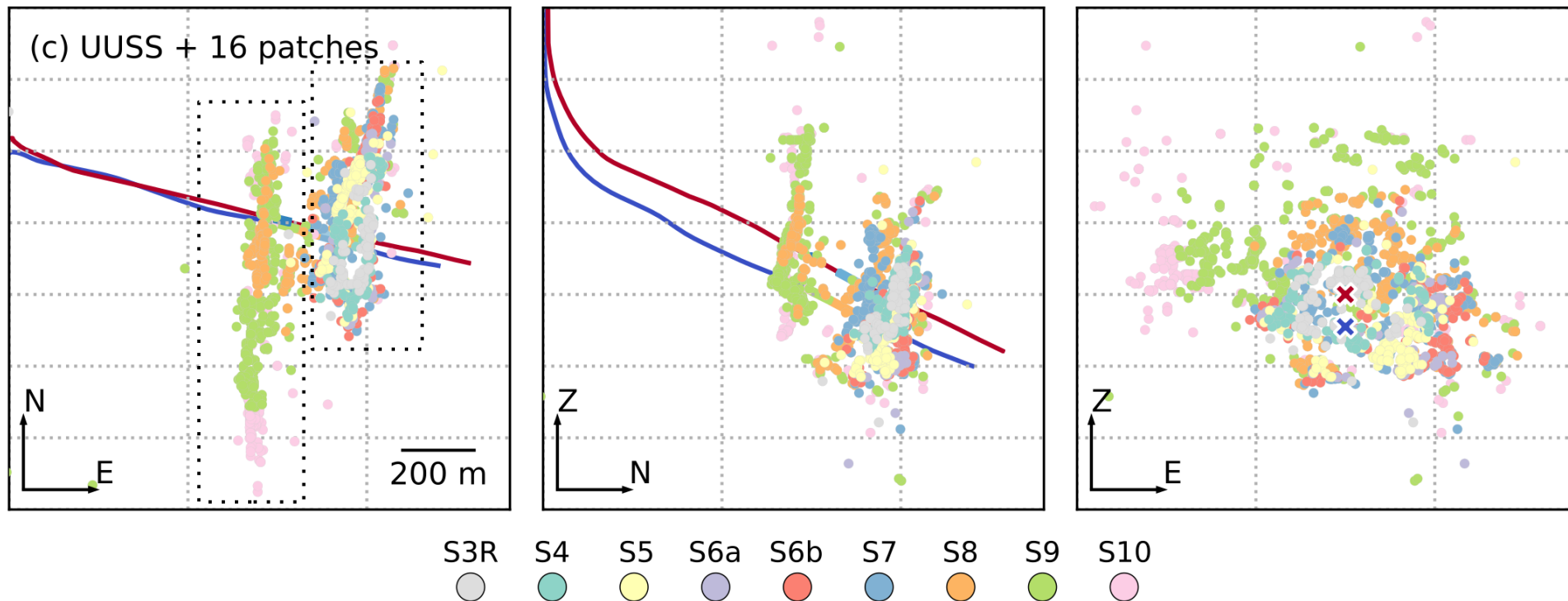
- permanent USSS (University of Utah Seismograph Stations)
- temporary geophone patches (3x3 nodal geophones)

→ excellent azimuthal coverage

→ improved SNR



Stimulations 2024 – Microseismic catalog



3000 microseismic events from surface monitoring catalog (Niemz et al., 2025)

→ MT inversion targets: 230 events ($M_L > 0$)

Methods - Probabilistic waveform-based MT inversion



Input

- Seismic waveforms

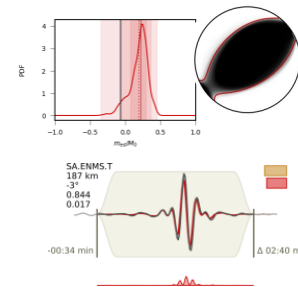


GROND

Probabilistic inversion $|d_{\text{obs}} - d_{\text{syn}}|$

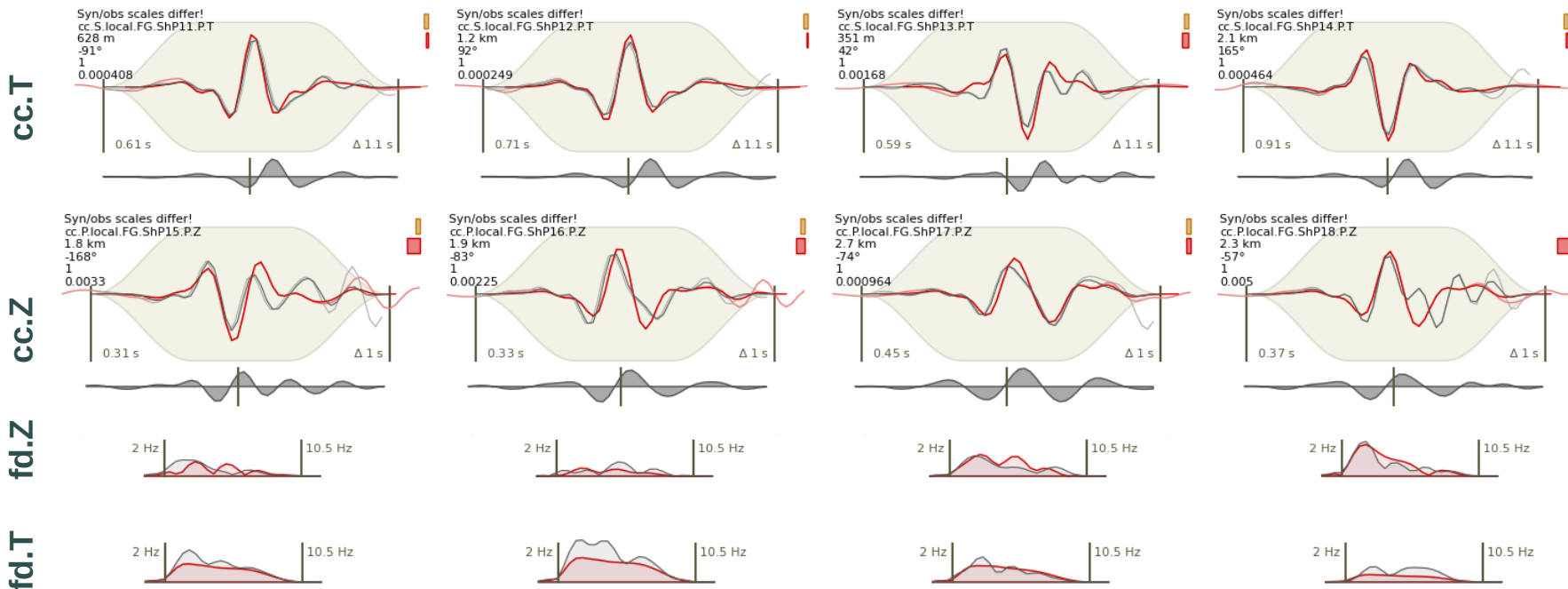
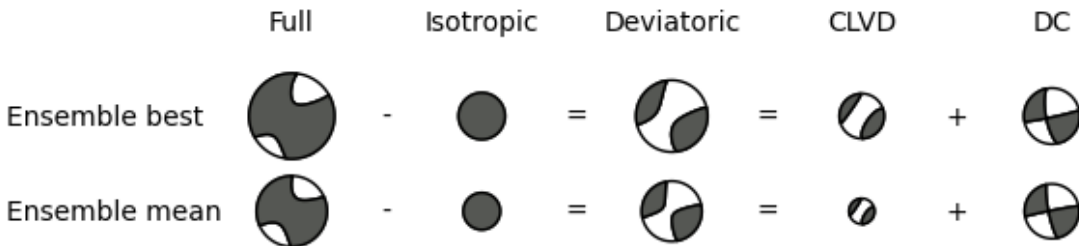
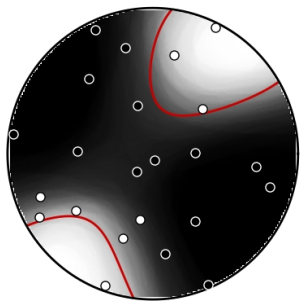
- Efficient exploration of the full model space
 - Bootstrap-based uncertainties
 - Parameter trade-offs
- Flexible design of misfit function:
 - FD Amplitude Spectra
 - TD Full waveforms
 - TD Cross-correlation of waveforms
 - Polarities

Output

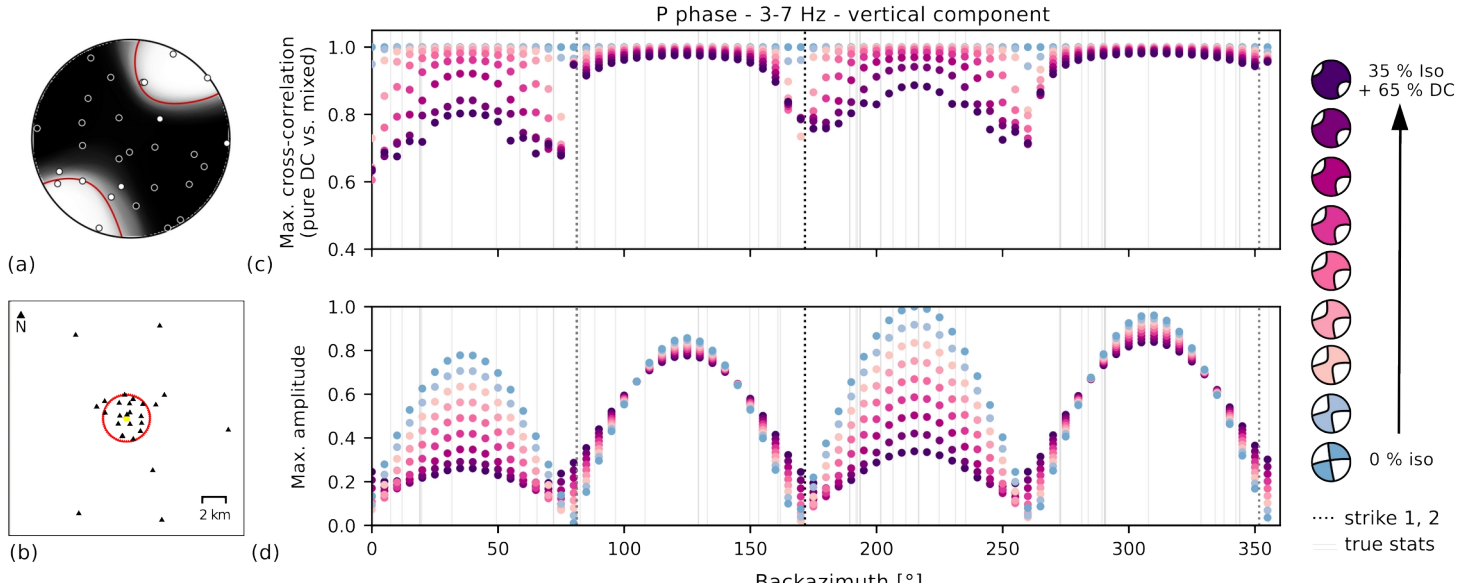


Pre-calculated Green's function data base

Stimulation 2024 - MT for example Mw 1.4

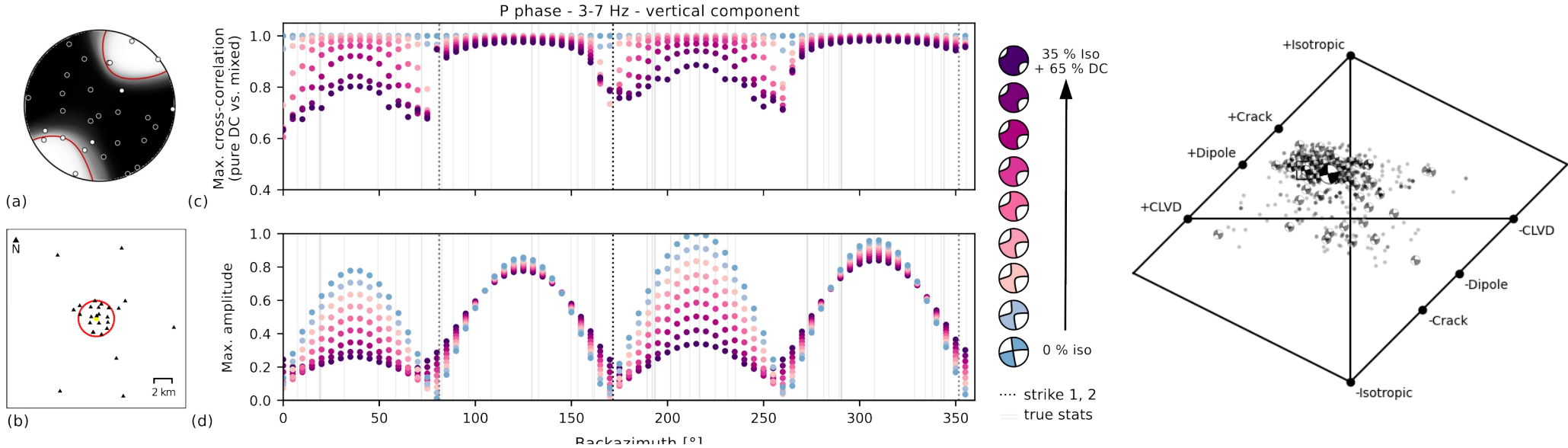


MT/Non-DC resolution testing + Uncertainties



- Comparison of synthetic waveforms with different isotropic contributions → Resolution tests

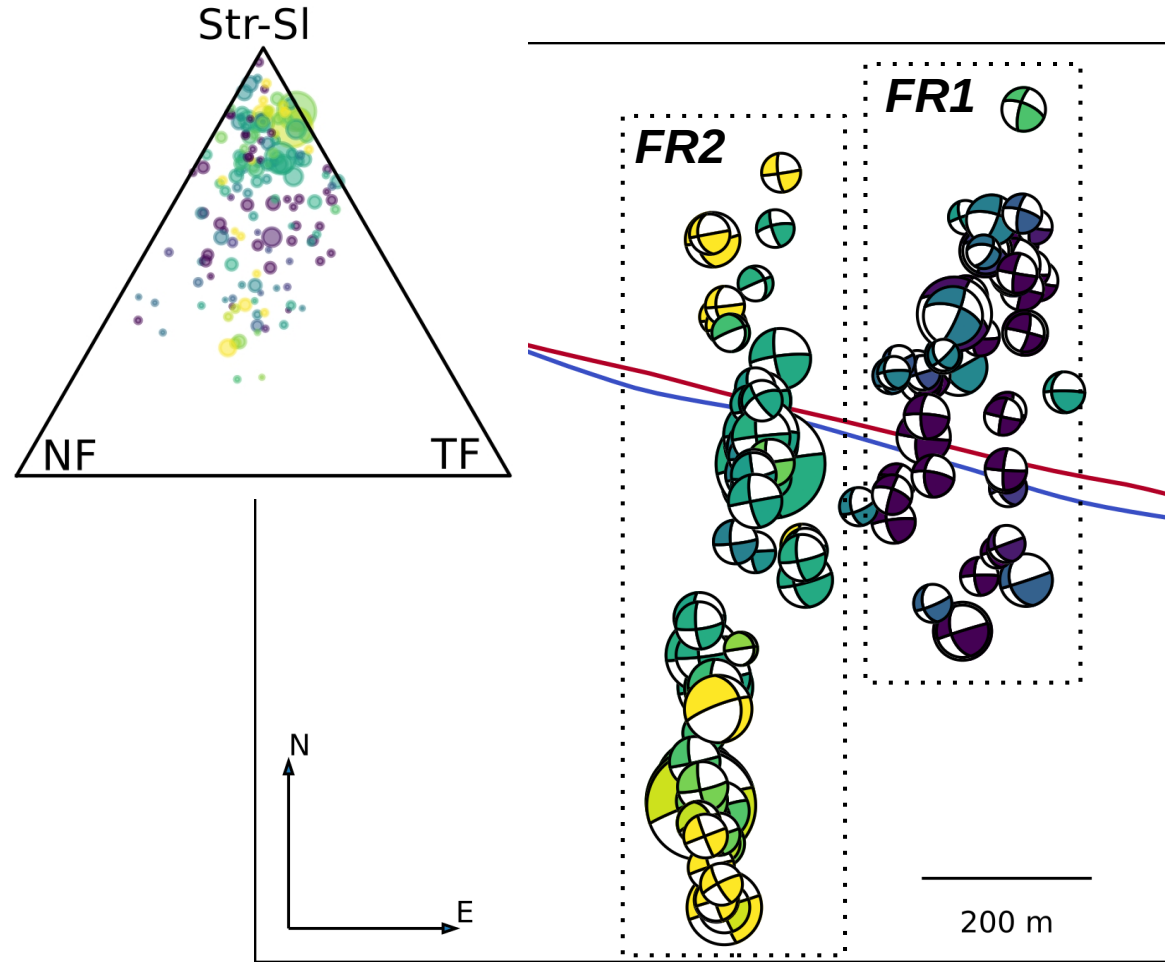
MT/Non-DC resolution testing + Uncertainties



- Comparison of synthetic waveforms with different isotropic contributions → Resolution tests
- Bootstrap chains → Uncertainties for all inversion parameters
- First-motion polarities → Validation

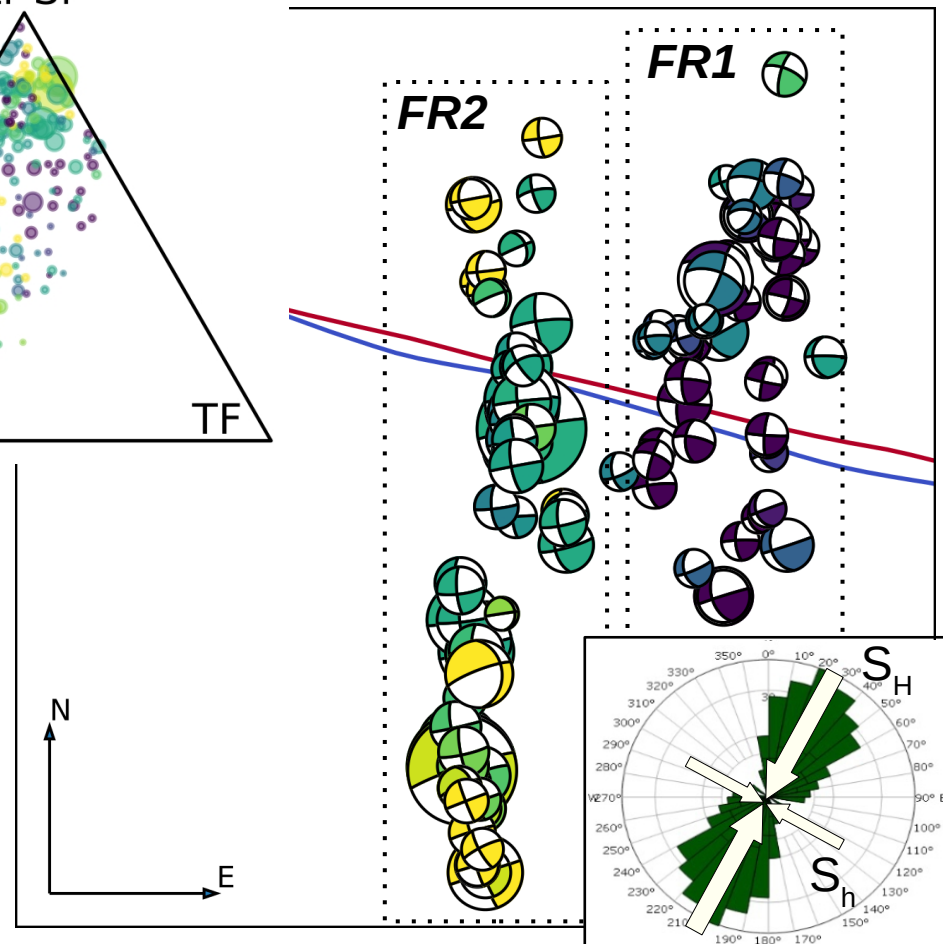
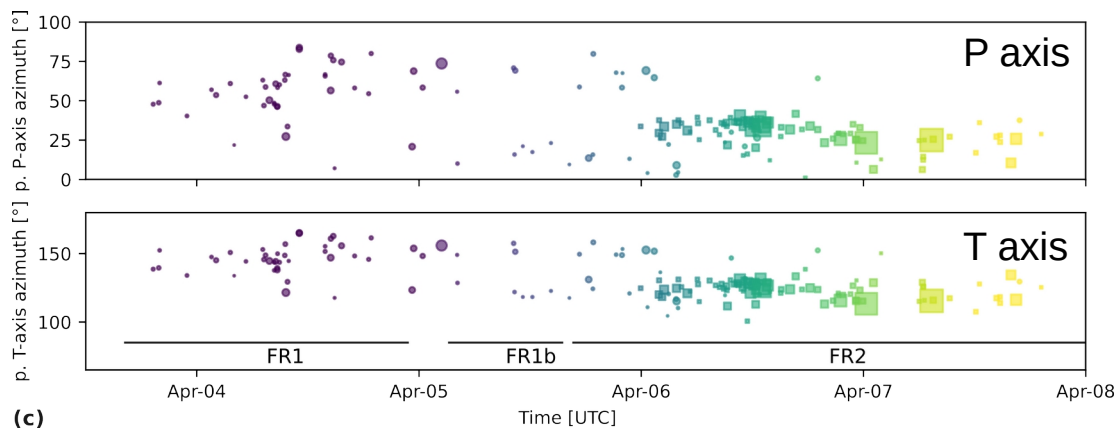
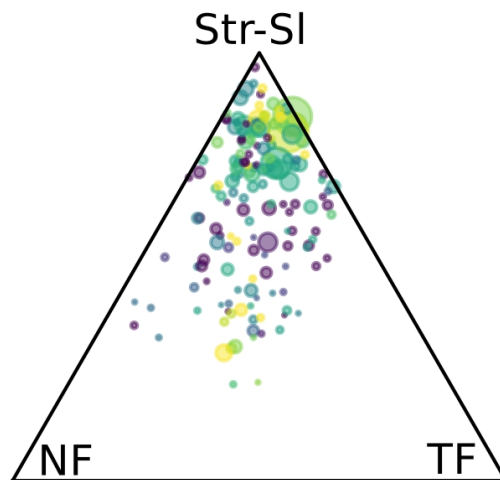
Stimulations 2024 – DC components

- 160 stable MT solutions
- predominately strike-slip



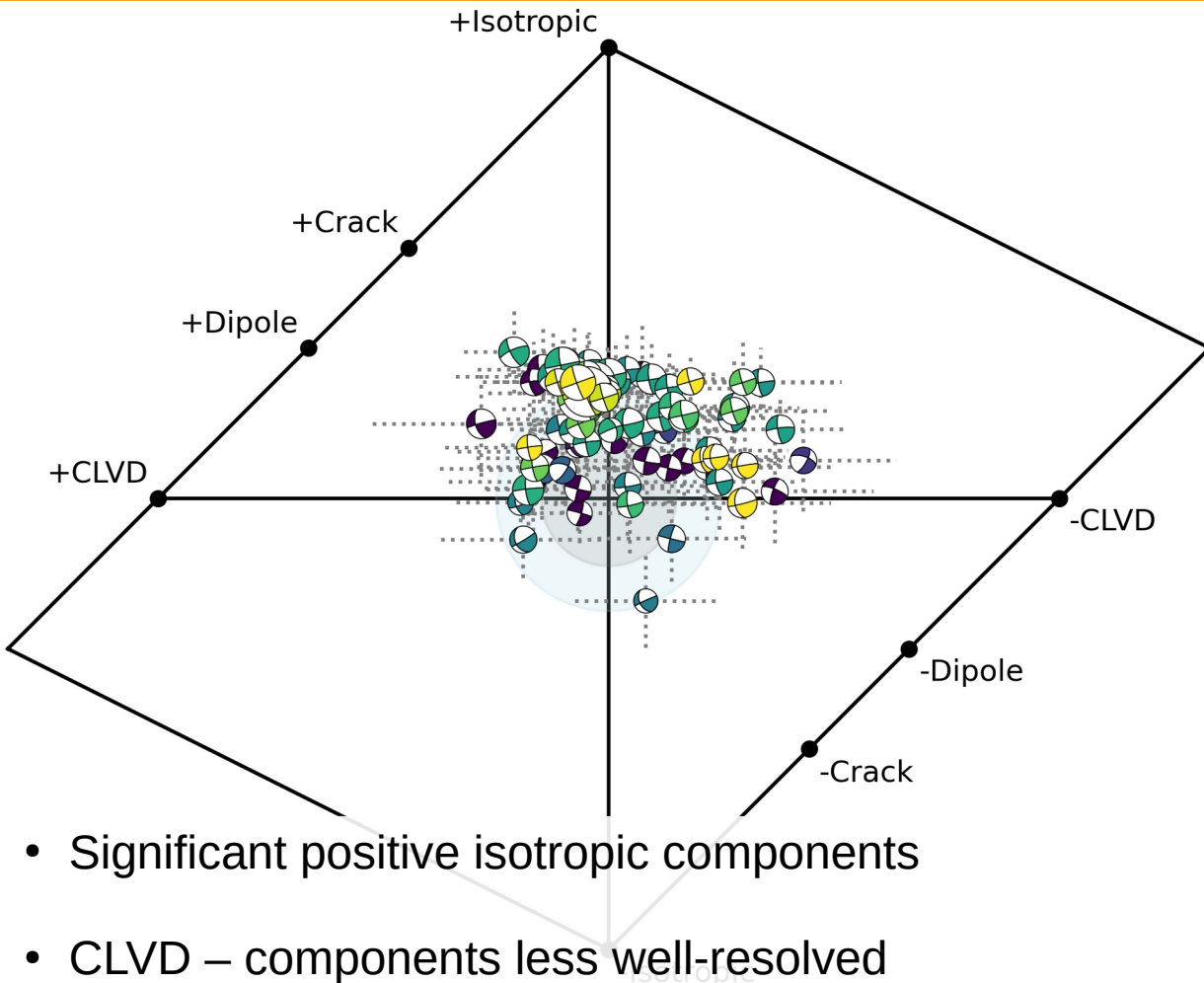
Stimulations 2024 – DC components

- 160 stable MT solutions
- predominately strike-slip
→ following regional stress field
- slight rotation from FR1 to FR2
→ nodal planes + microseismic cloud

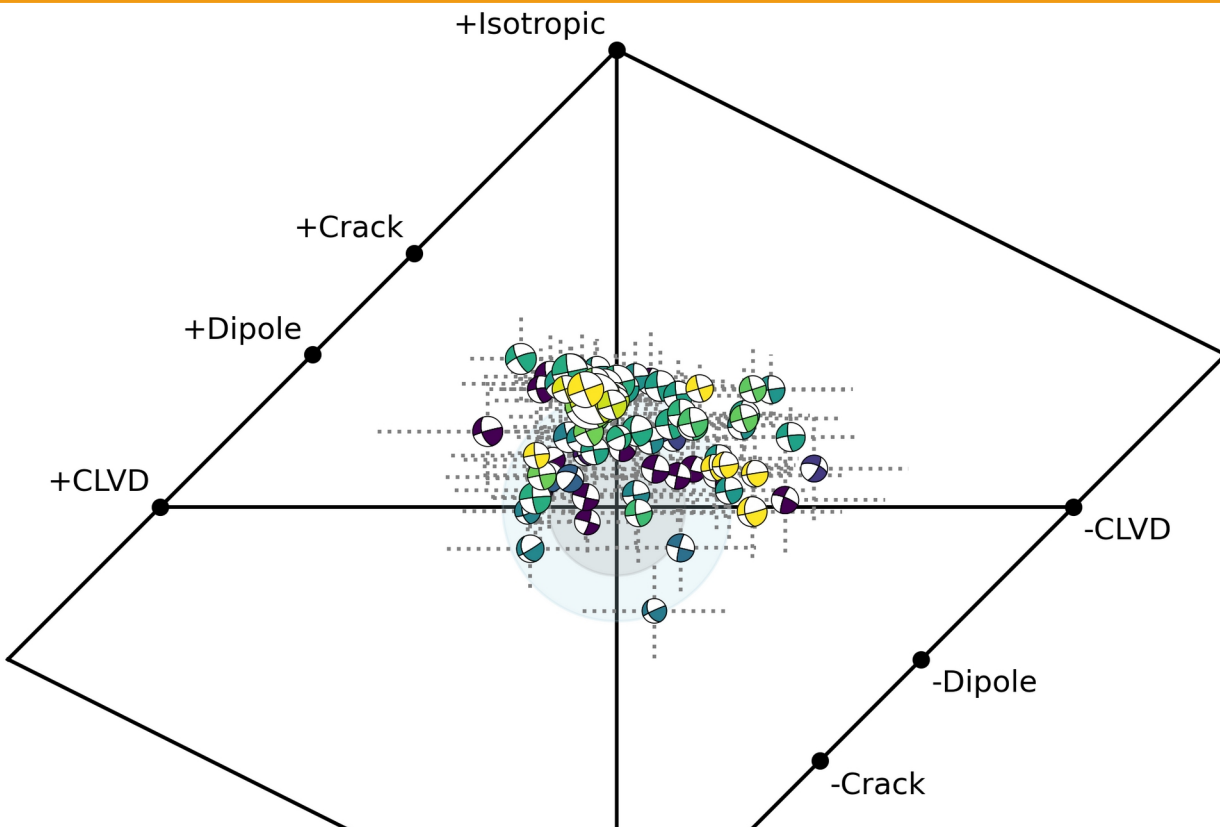


Induced fractures in well 58-32 (Nadimi et al. 2020)

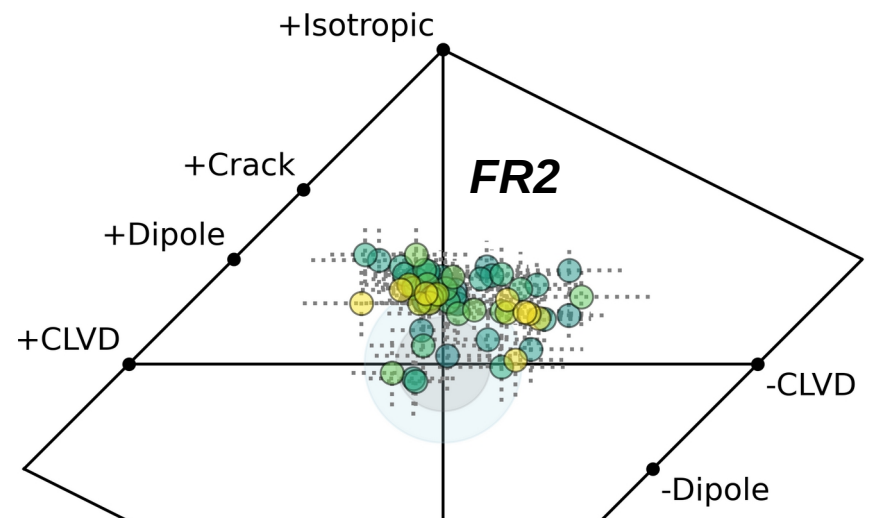
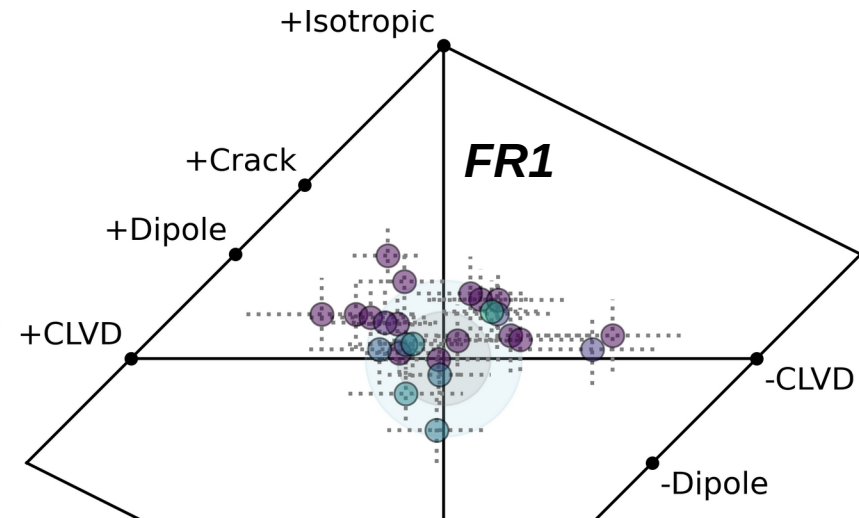
Stimulations 2024 – Non-DC components



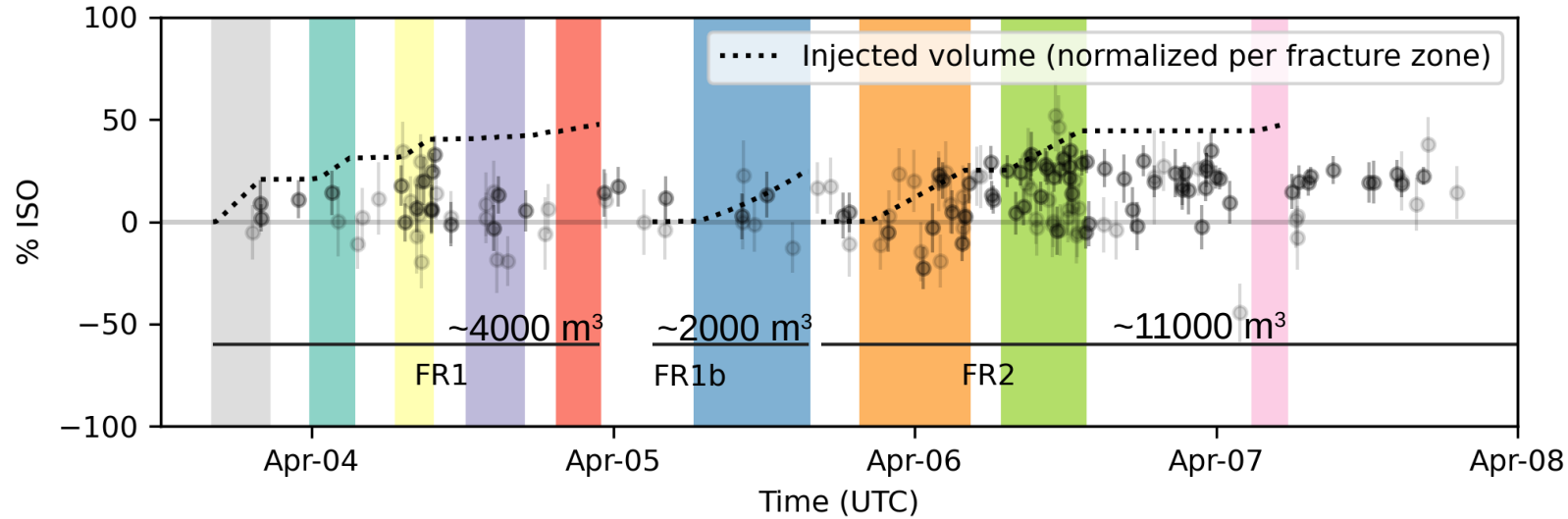
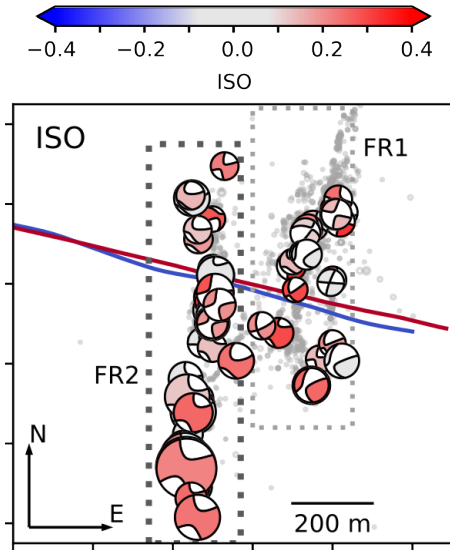
Stimulations 2024 – Non-DC components



- Significant positive isotropic components
- CLVD – components less well-resolved



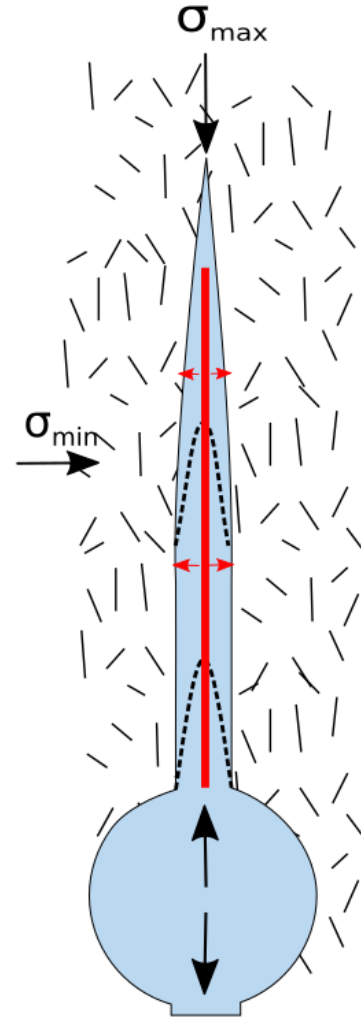
Stimulations 2024 – Isotropic component



- Significant positive isotropic components

→ Maximum ISO - contribution increases over time / with injected volume
(no bleed-off during in between stimulation stages)

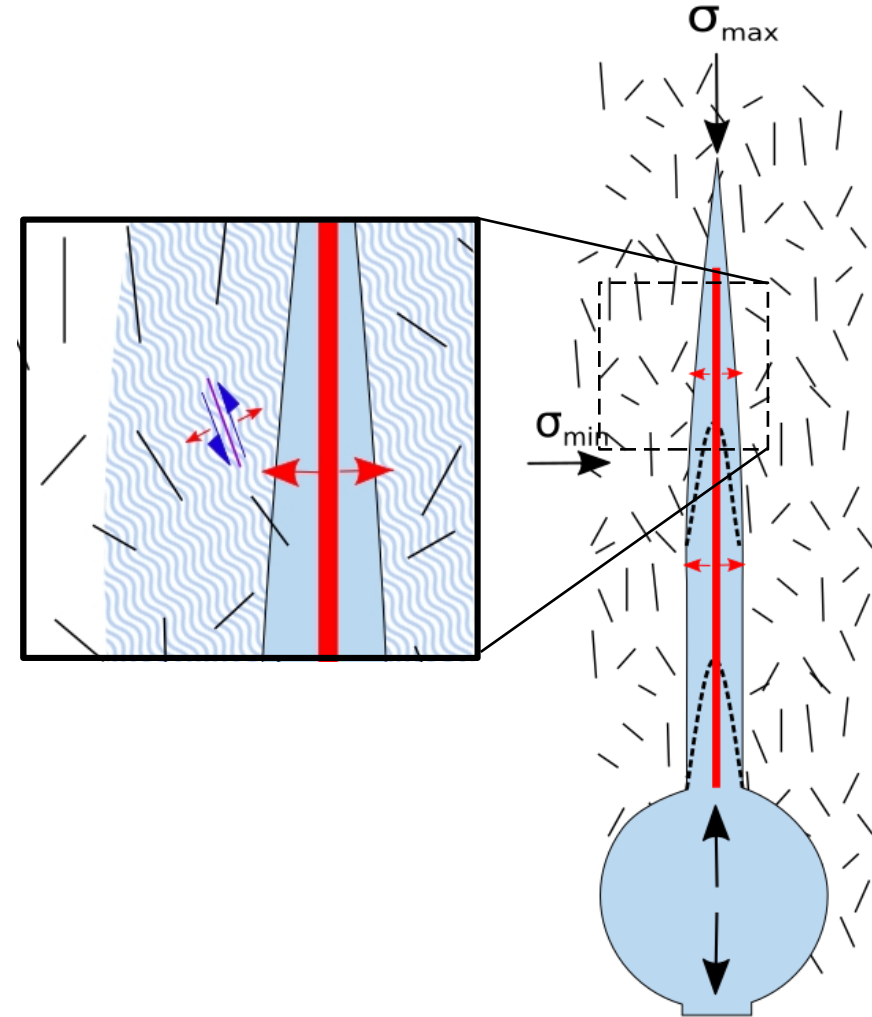
Conceptual models



Conceptual models

ISOTROPIC components

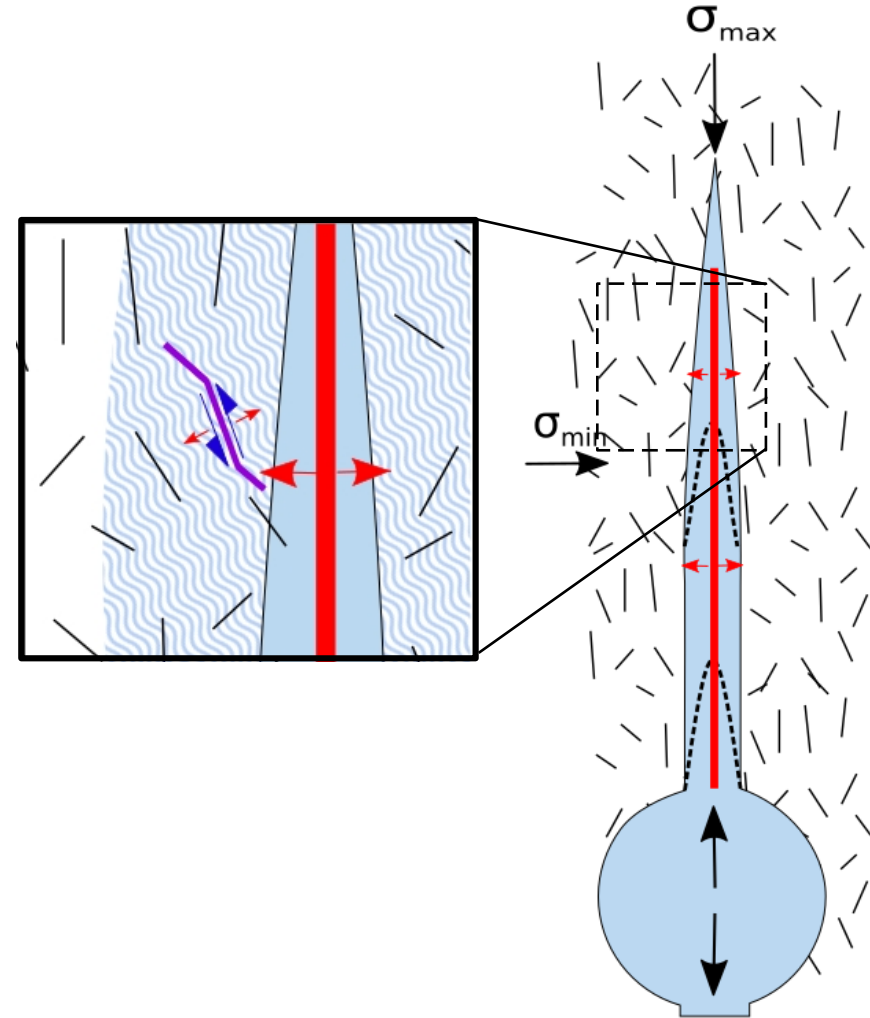
- (1) leak-off into rock around hydraulic fracture
- (2) increased pore pressure
→ reduced normal stress
- (3) opening possible
→ larger isotropic contributions
with increasing volume



Conceptual models

CLVD components

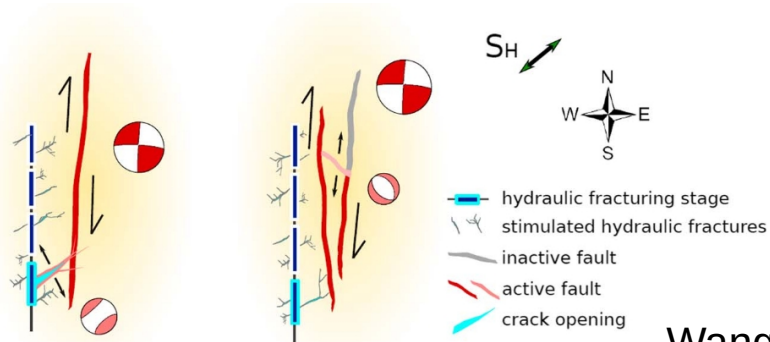
- Resolution limits:
 - fault complexity, fracture jogs
 - inadequacies of velocity model



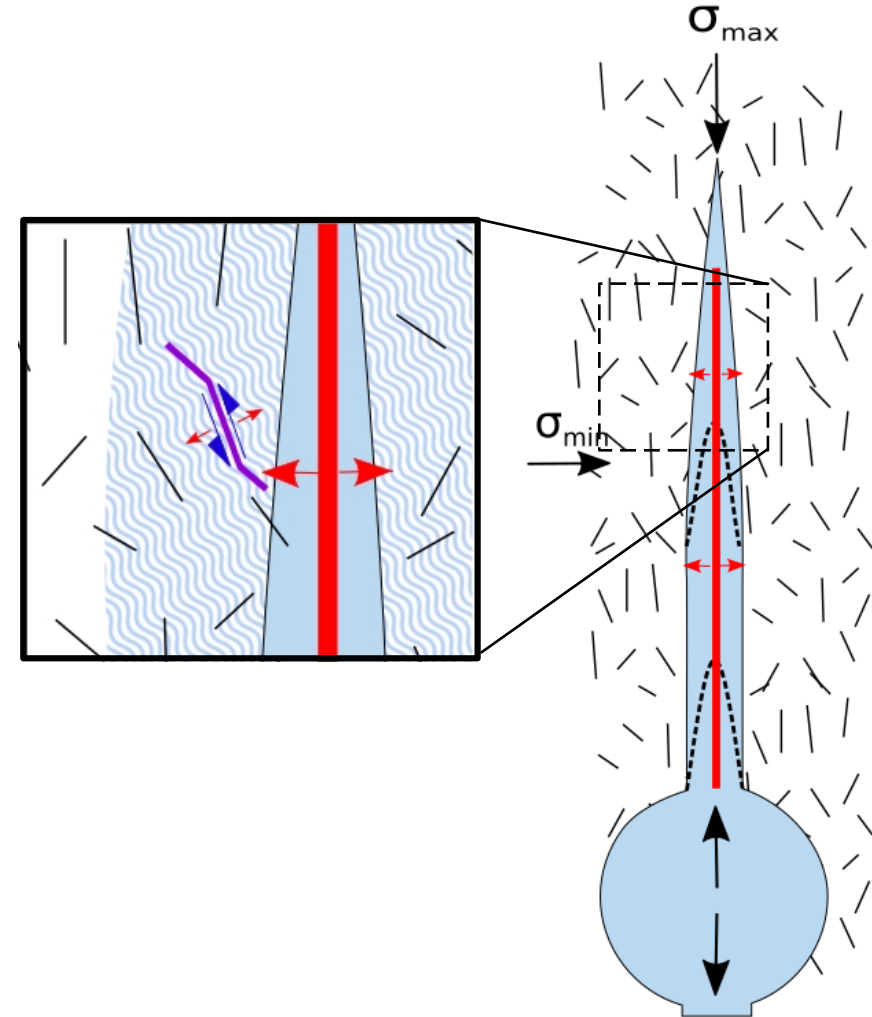
Conceptual models

CLVD components

- Resolution limits:
 - fault complexity, fracture jogs
 - inadequacies of velocity model
- alternative decomposition:
 - major + minor DCs



Wang et al., 2018



Conclusion → Questions

- Dominate strike slip in agreement with stress conditions during the 2024 stimulation
 - incl. significant positive isotropic components
 - isotropic components increase with injected volume

Are increasing isotropic component of MTs a proxy for a more efficient fracture network?

or

What is the role of slip-dominated microseismicity in the creation of an efficient EGS?



THANK YOU

McClure and Horne (2014): An investigation of stimulation mechanisms in Enhanced Geothermal Systems. International Journal of Rock Mechanics & Mining Sciences (72), 242–260.

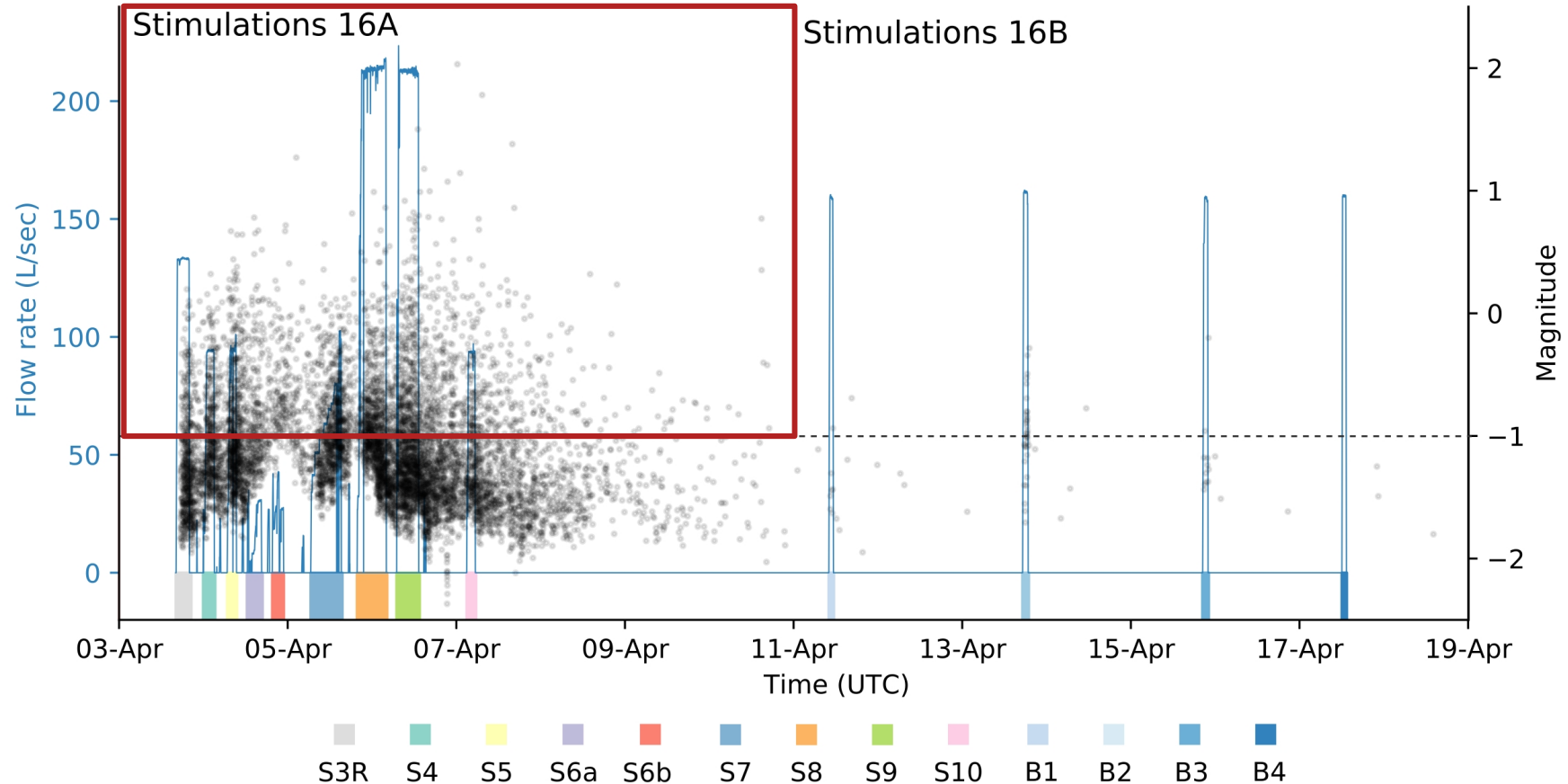
Nadimi et al. (2020): Utah FORGE: Hydrogeothermal modeling of a granitic based discrete fracture network. Geothermics, 87, 101853.

Niemz et al. (2025): Mapping Fracture Zones with Nodal Geophone Patches: Insights from Induced Microseismicity During the 2024 Stimulations at Utah FORGE. SRL.

Wang et al. (2018): Faults and non-double-couple components for induced earthquakes. Geophysical Research Letters, 45.

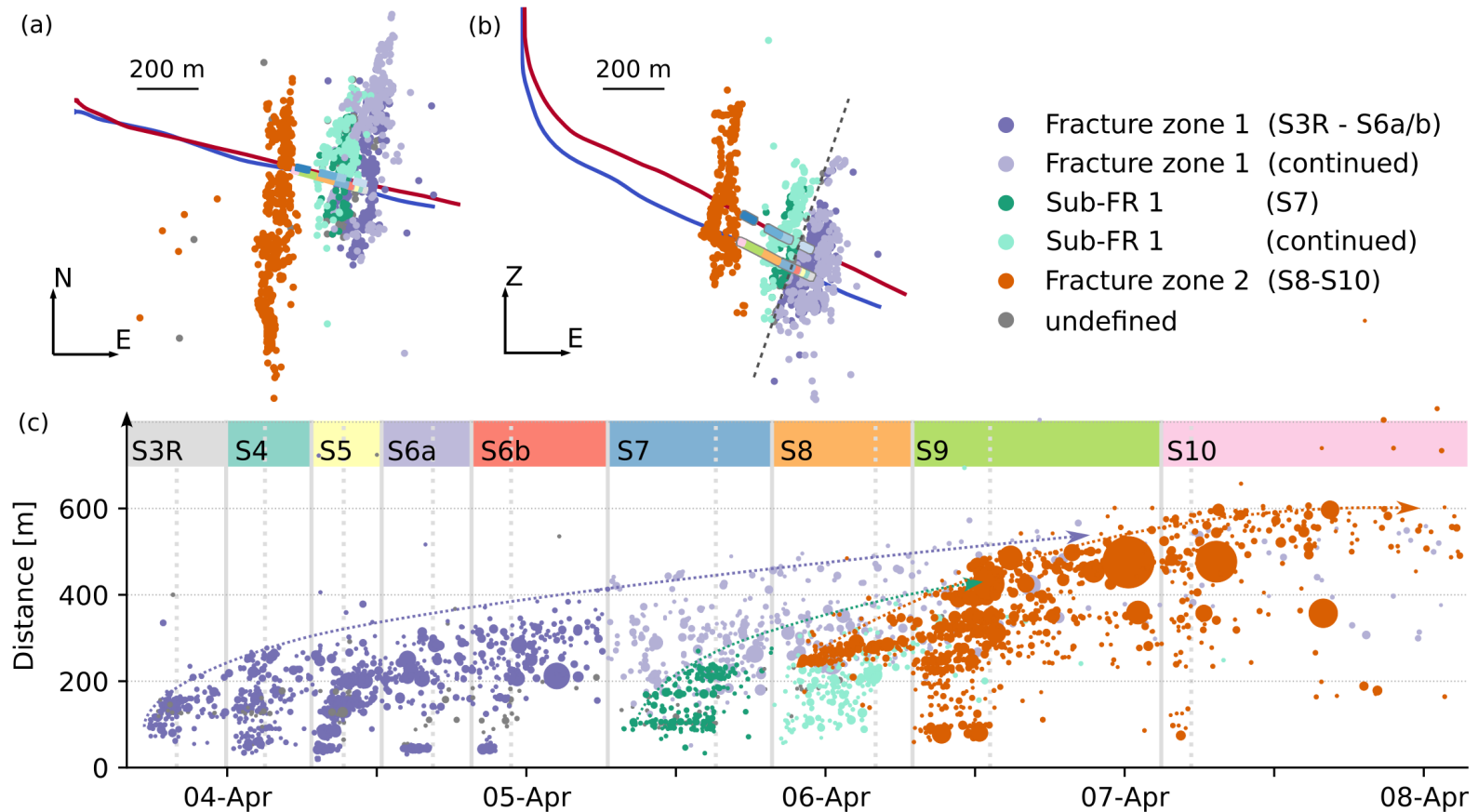
Funding provided by the US DoE with additional support from Utah Trust Lands Administration, Beaver County, the Governor's Office of Energy Development, and Smithfield Foods.

Stimulations 2024 – Microseismic catalog



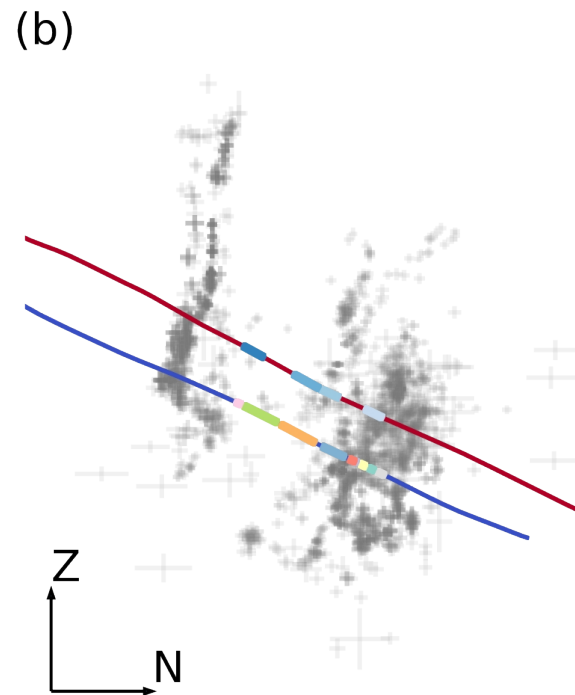
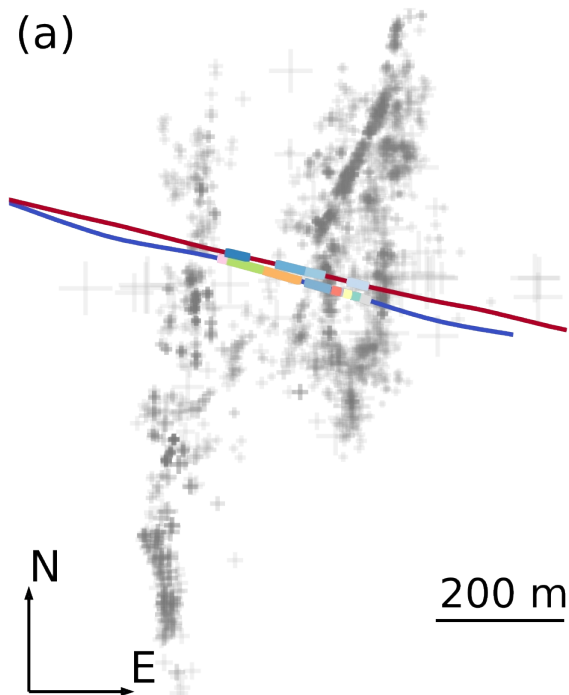
Surface monitoring catalog (Niemz et al., 2025)

Stimulations 2024 – Flow pathes



→ Pathways for fluid flow during the August/September circulation tests between the wells

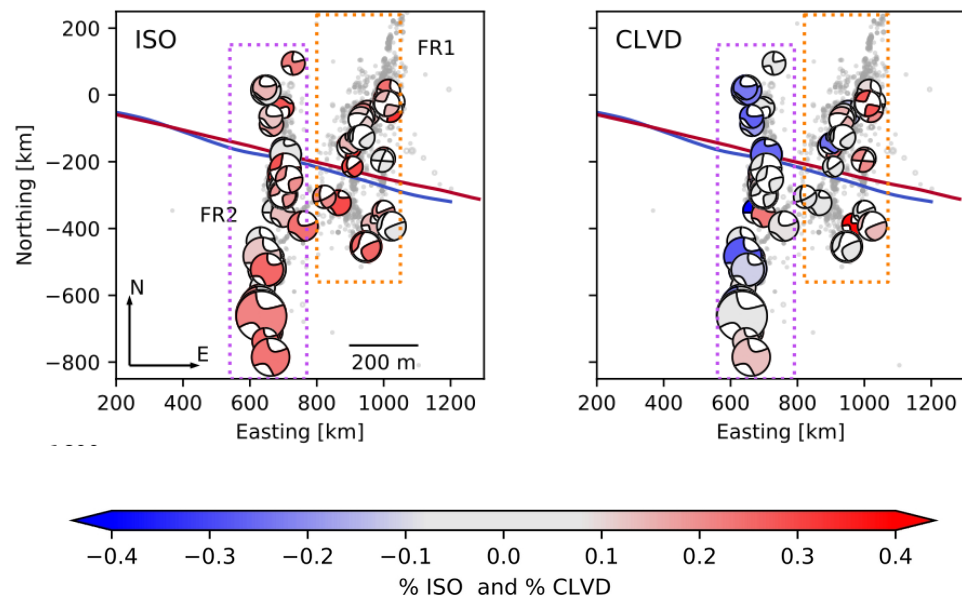
Utah FORGE 2024 – Location uncertainties



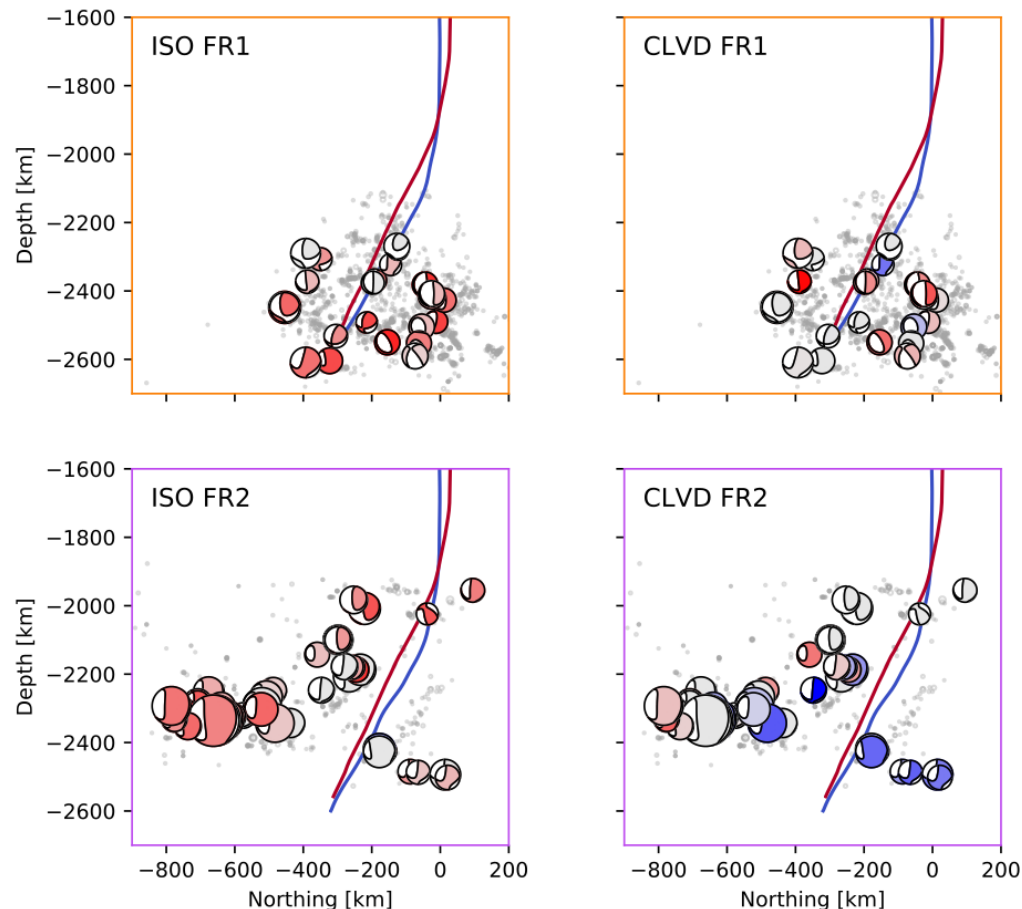
Based on 100 bootstrap solutions in GrowClust

Stimulations 2024 – Non-DC components

Map views



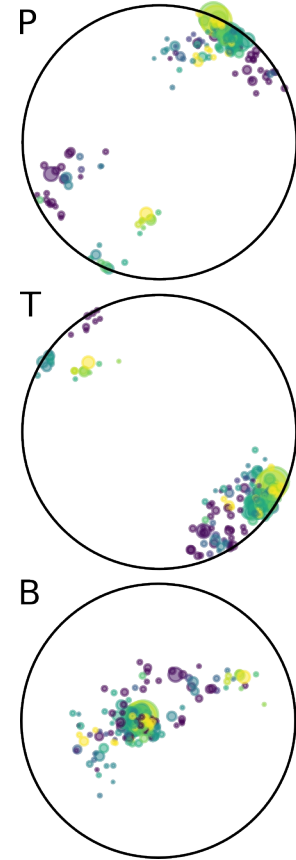
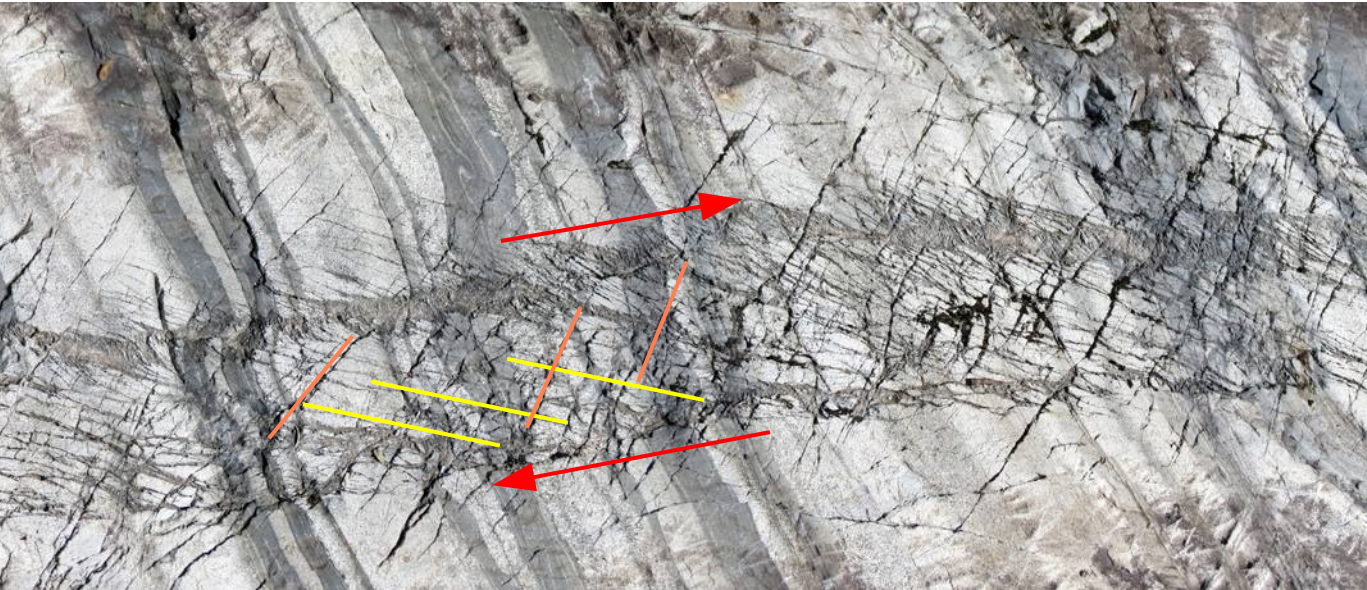
Depth sections



- Significant positive isotropic components
- CLVD – components less well-resolved

Strike slip dominance with rotated slip axes

- a) preexisting small scale fractures/faults with small variations in strike
- b) Riedel shear



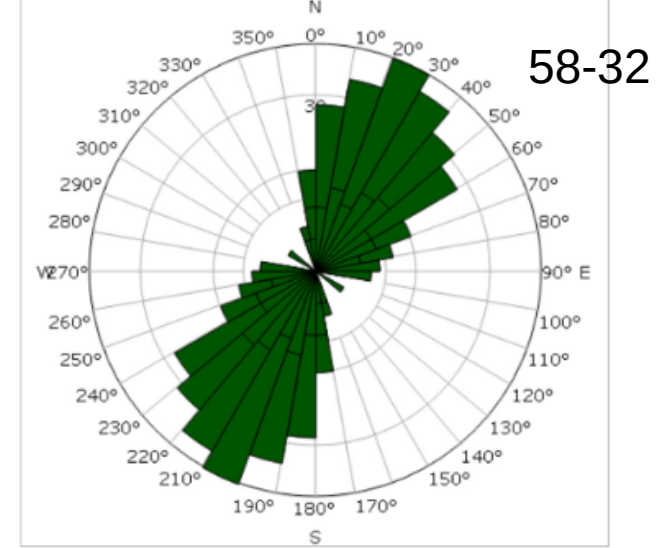
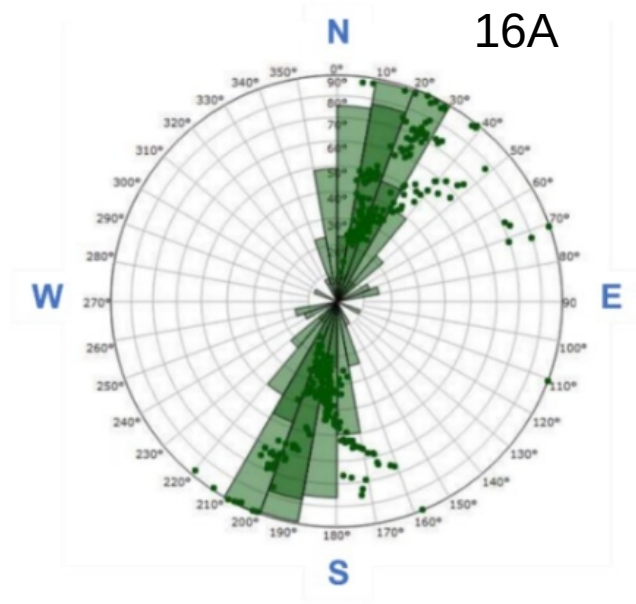
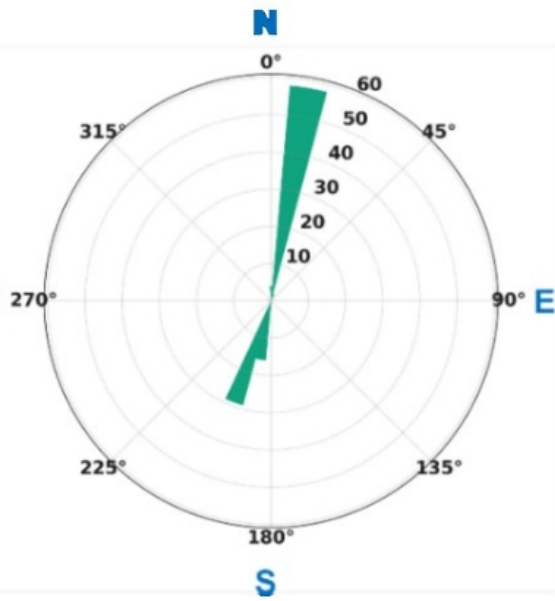
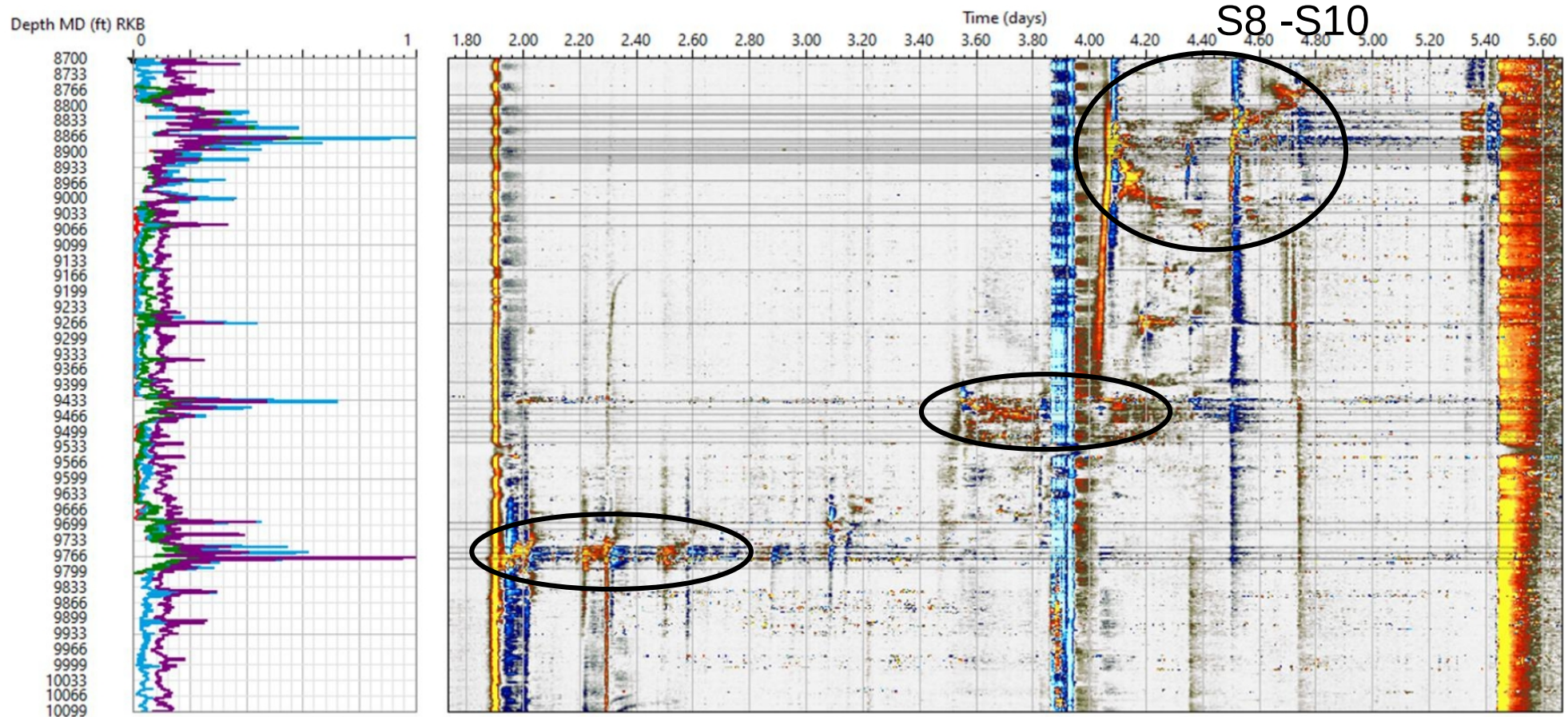


Fig. 10. Well 58-32 rose plot. This plot represents the drilling induced fracture sample set from the actual FMI fractures ranging from 968-2297 m measured depth.

Figure 5: (a) The azimuth of drilling-induced fractures in deviated well 16A(78)-32, inferred from the stress inversion using Method 2, suggests that the orientation of S_{Hmax} ranges from N5°E to N30°E. (b) The azimuth of drilling-induced fractures in deviated well 16A(78)-32, observed from the image logs, suggests that the orientation of S_{Hmax} ranges from N10°E to

Stimulations 2024 - Frac hits at 16B measured via fiber optics



S3 -S5/S6

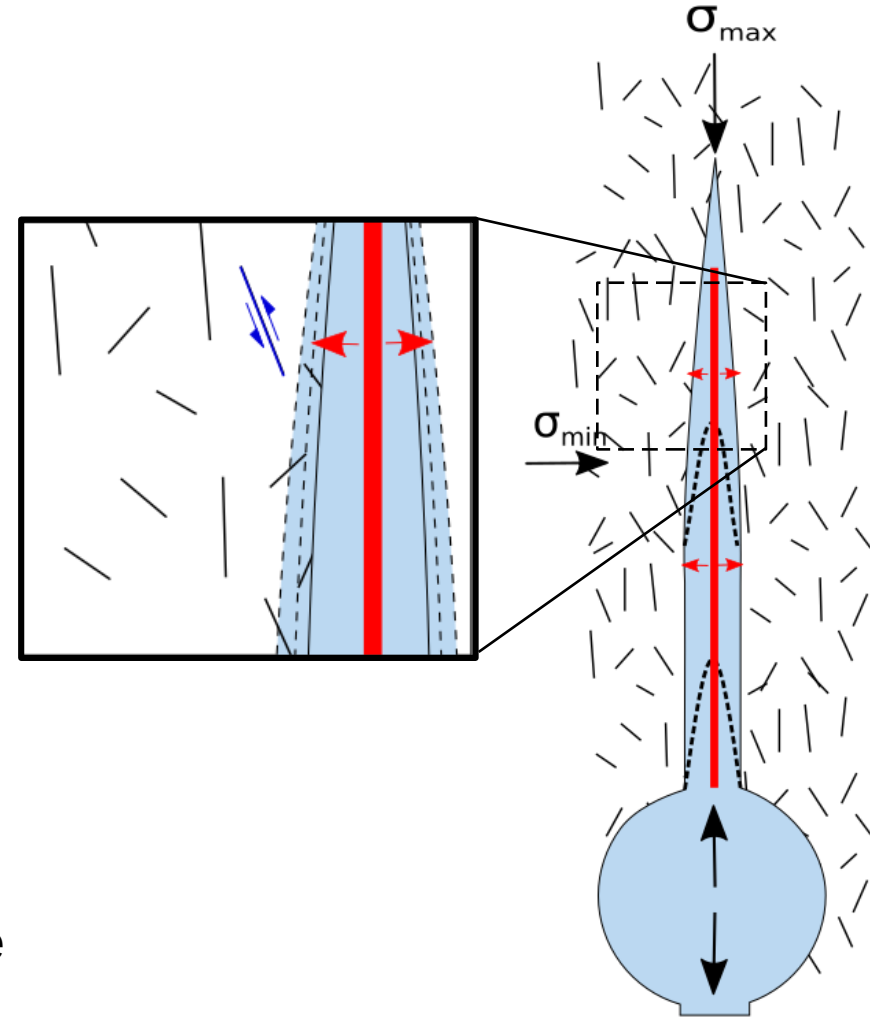
UTAH FORGE
EVO2 - 16A FRAC
16B RFS DSS Strain Change Rate



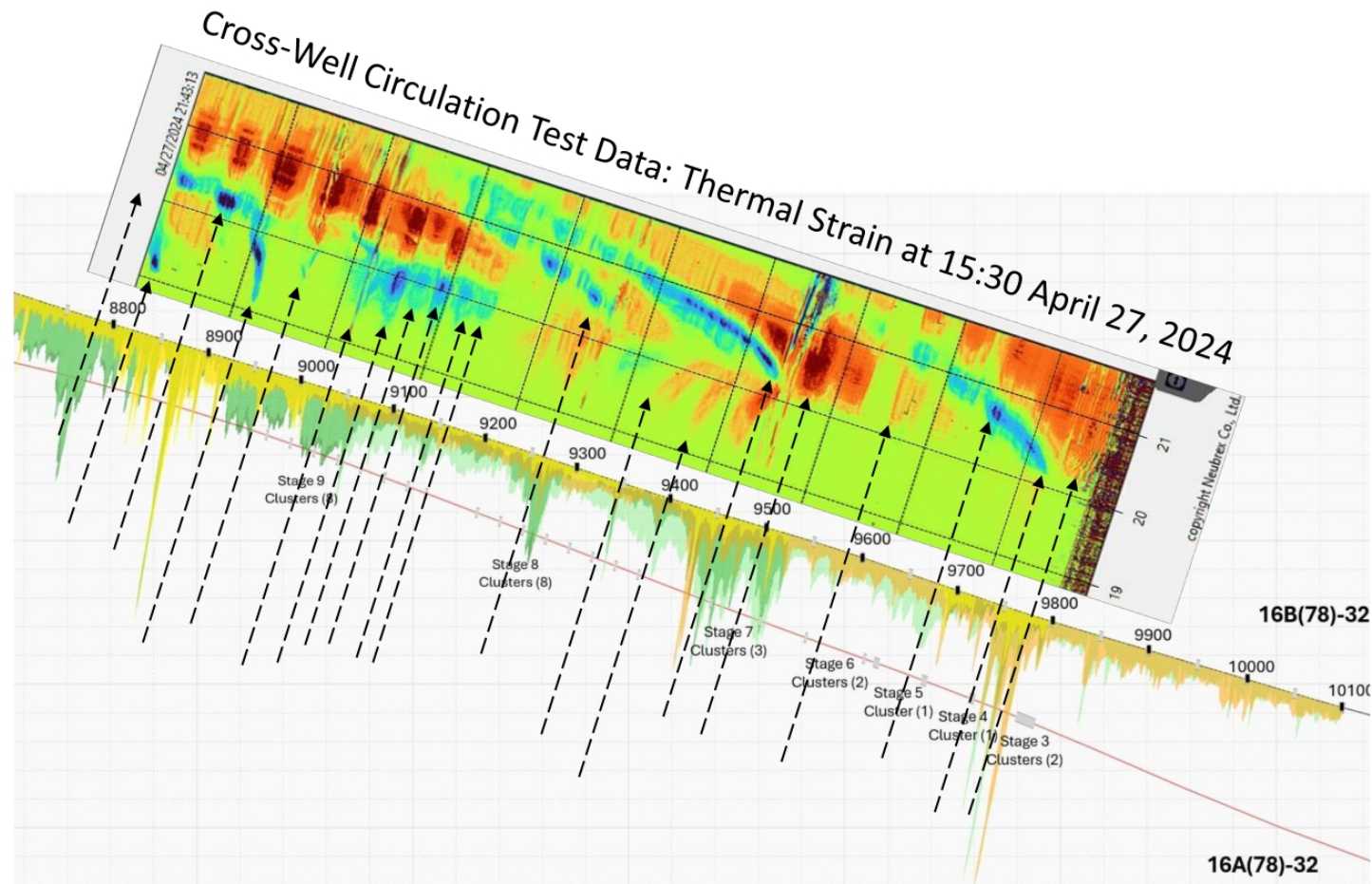
Conceptual models

ISOTROPIC components

- (1) slip along preexisting fracture in the fracture wall
- (2) quasi-instantaneous marginal opening of the HF
- (3) composite signal from two sources close in space



Utah FORGE 2024 – DAS-based Frac Hits



16B(78)-32 Fracture
Driven Strain

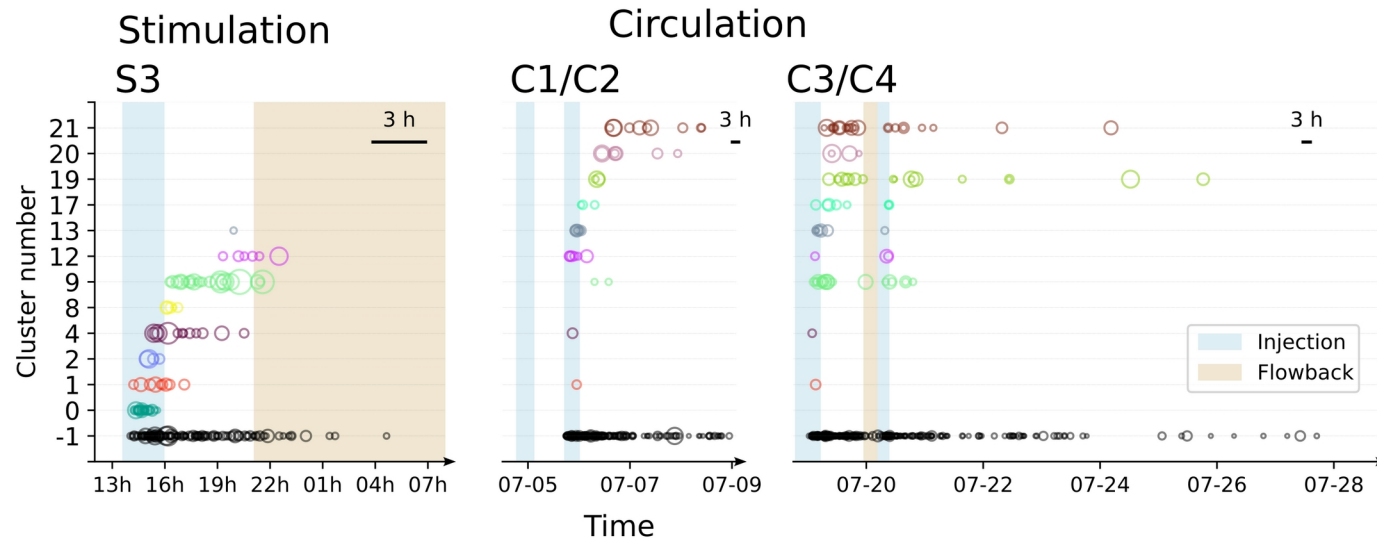
16A(78)-32 Frac Stages

Courtesy of Neubrex

Event similarity

Repeated activation and newly activated volumes

- Applying **waveform-based** earthquake clustering (*Clusty*, Petersen and Niemi, et al., 2021)
- Combining stimulation and circulation
 - identifying overlapping activity + new clusters



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