

Schweizerischer Erdbebendienst  
Service Sismologique Suisse  
Servizio Sismico Svizzero  
Swiss Seismological Service

**ETH** zürich

# Direct measurements of asperity evolution in the laboratory relating to fault reactivation in stimulated reservoirs

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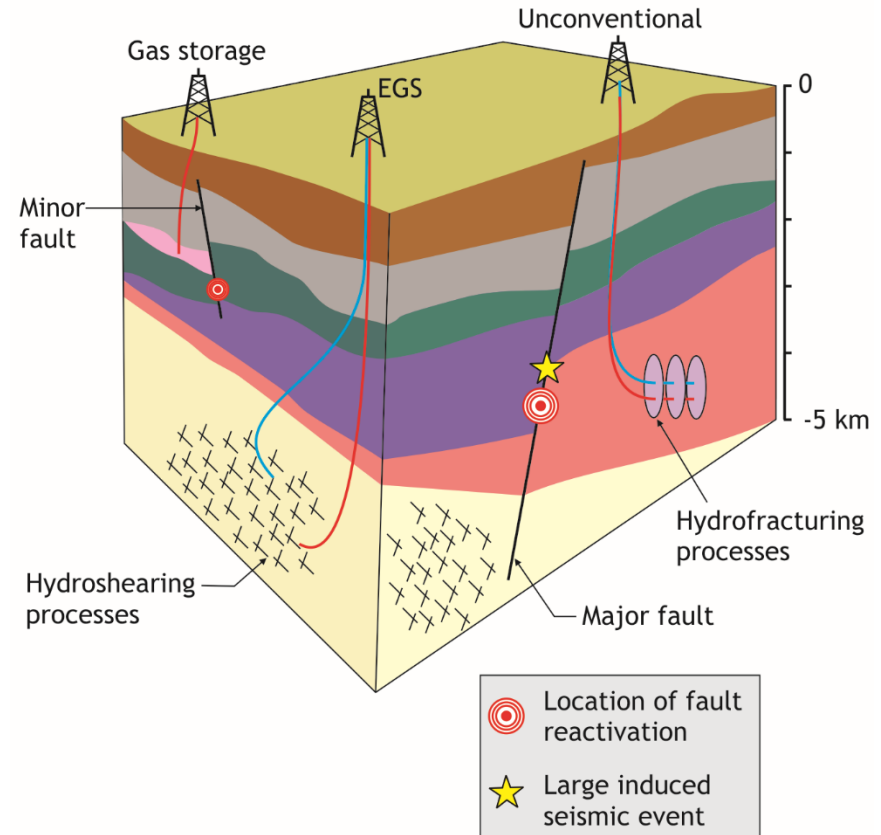
*<sup>2</sup>University of California, Berkeley*

Schatzalp Workshop on Induced Seismicity  
Davos, Mar. 16, 2017

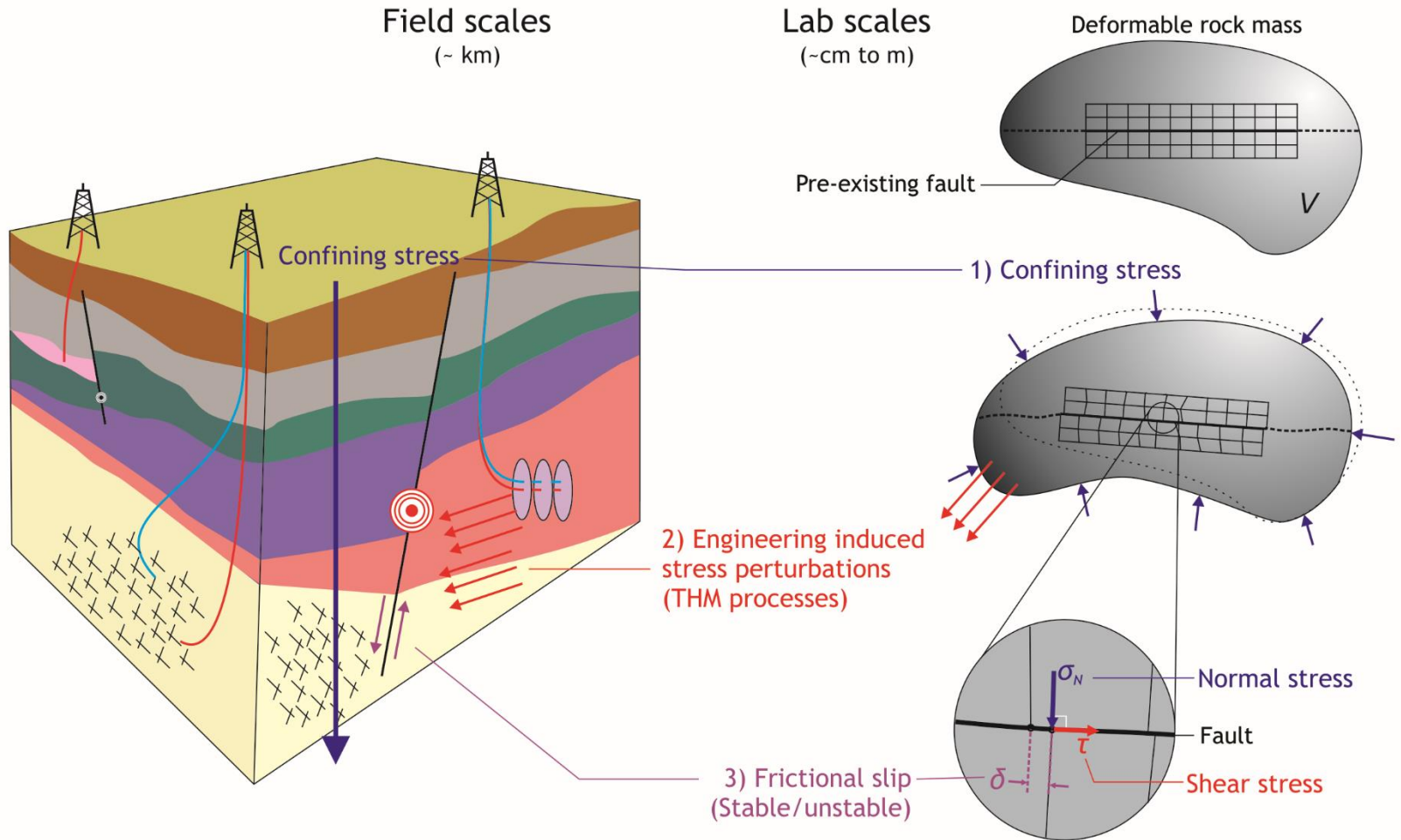
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## Motivation

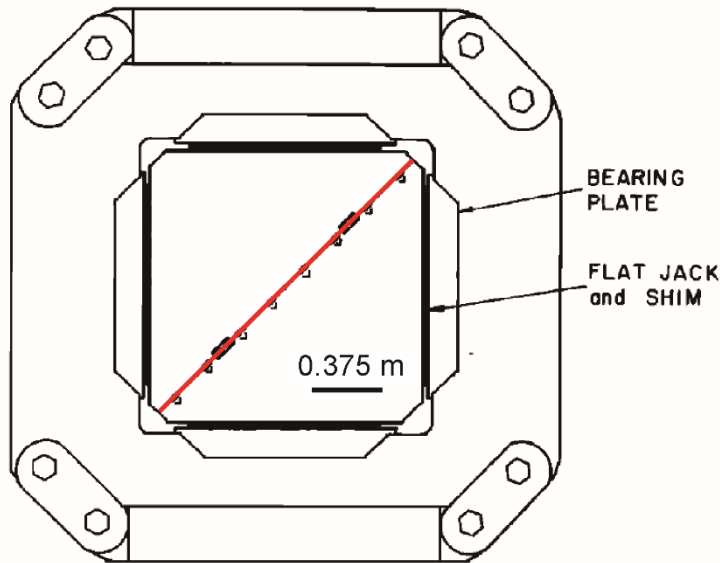
- **Reactivation of natural faults** can lead to **induced seismicity** and is a byproduct of a variety of subsurface engineering activities:
  - *Oil and gas production*
  - *CO<sub>2</sub> storage*
  - *Shale gas extraction*
  - *Enhanced Geothermal Systems*
  - *Mining activities*
  - *Impoundment and dam stability*
- Determining the **hazard** associated with fault **reactivation** requires an understanding of the relationship between:
  - **Subsurface rock deformation,**
  - **frictional faulting,**
  - and **seismicity.**



# Background: Frictional laboratory studies

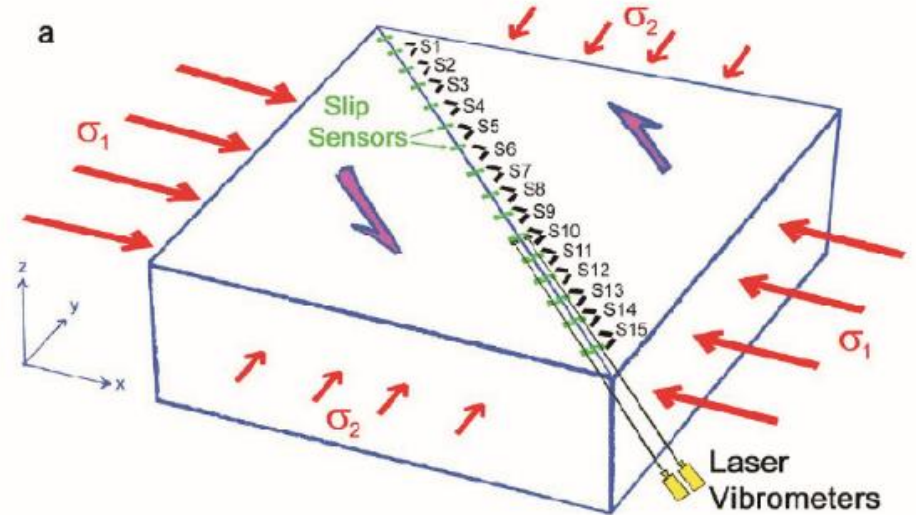
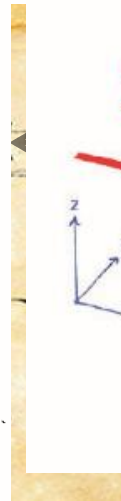


# Background: Frictional laboratory studies



- ∨ STRAIN GAGE
- VELOCITY TRANSDUCER
- ▬ DCDT DISPLACEMENT TRANSDUCER

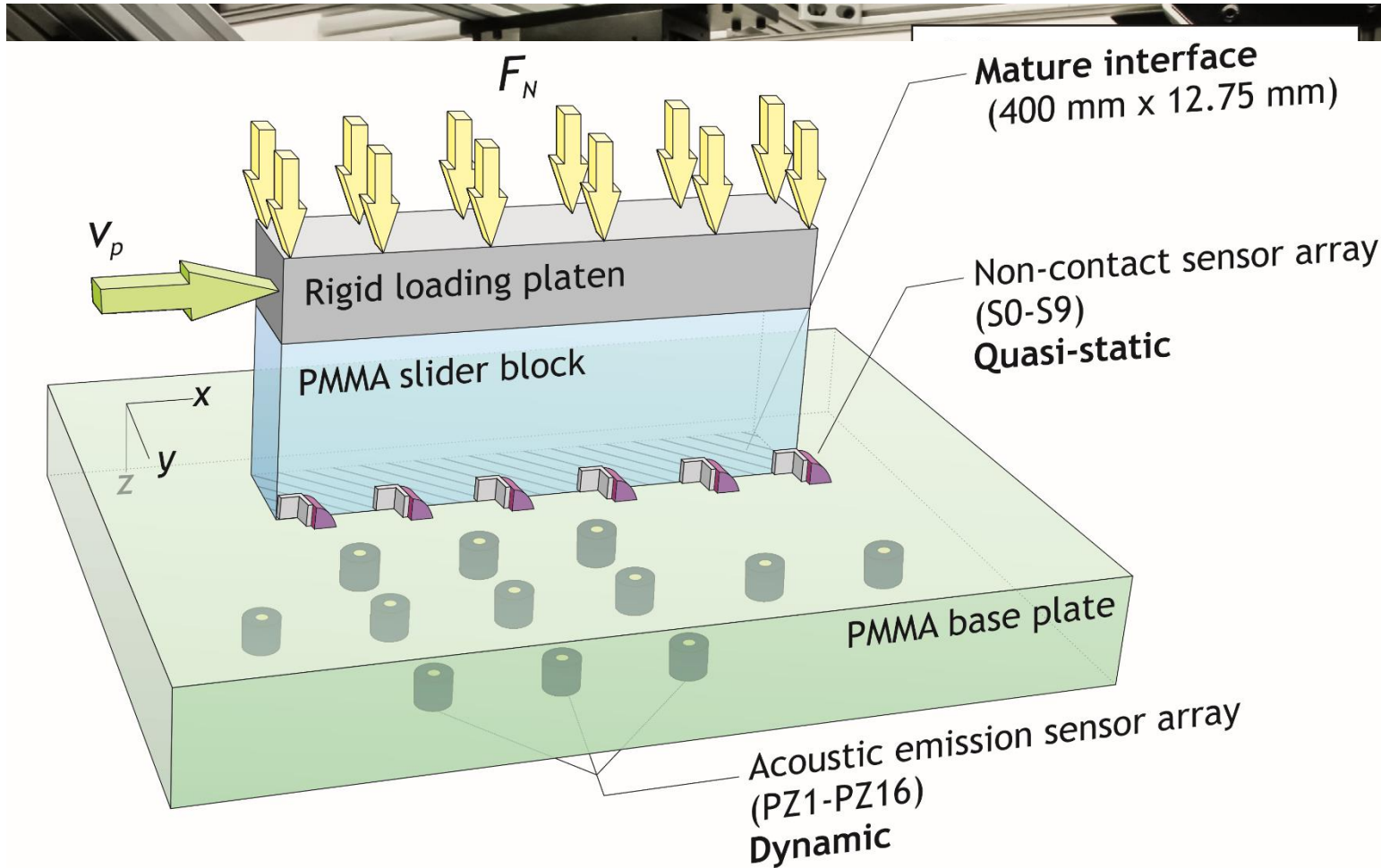
Leonardo da Vinci (ca. 1493)  
 Biaxial press  
 USGS, Menlo Park, CA  
 Dieterich (1978)



Biaxial press  
 USGS, Menlo Park, CA  
 McLaskey et al. (2015)

37 years

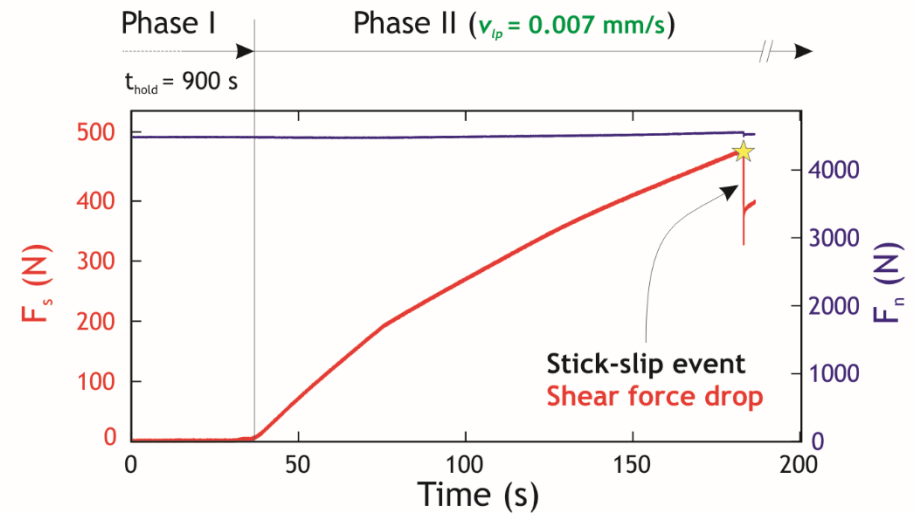
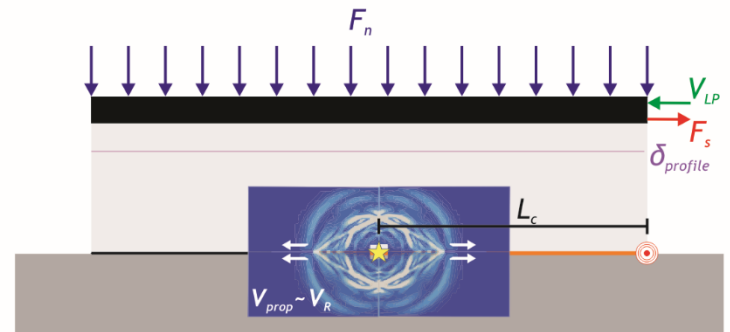
## UC Berkeley Direct Shear Friction apparatus



**PMMA** (Polymethyl methacrylate)

## Direct shear experimental procedure

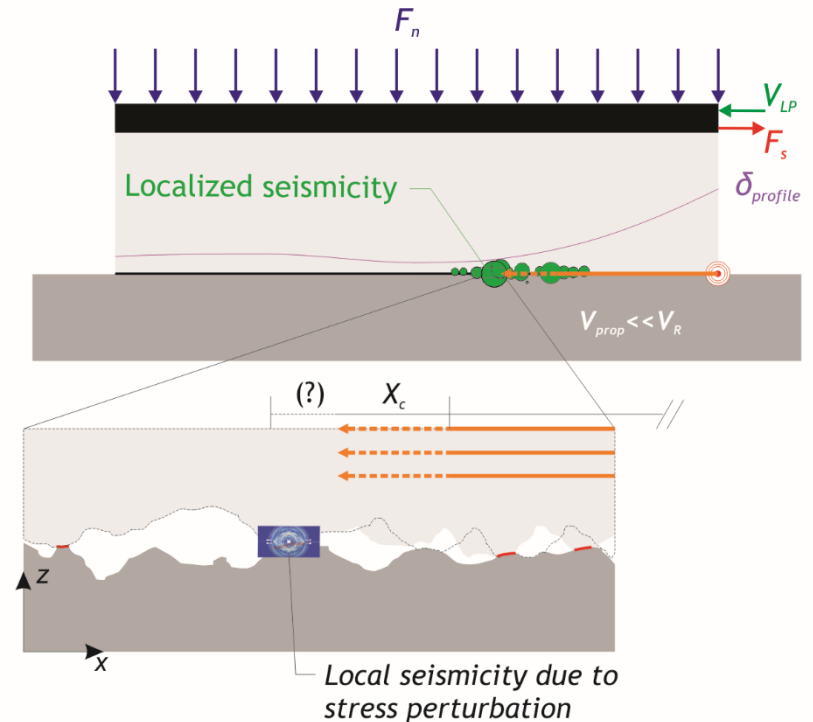
1. Mature **interface** is created between a slider block and base plate
2. Phase I: Normal force  $F_n$  is applied to the fault for  $t_{hold} = 900$  s
3. Phase II: Loading platen driven at a constant velocity  $V_{LP}$ . **Fault becomes reactivated**
  - i. **Shear rupture expands steadily** and is determined by the “kink” in the slip profile ( $\delta_{profile}$ ).
  - ii. **Localized seismicity** is observed when rupture front enters a specific section of the fault
  - iii. Upon reaching a *critical size* ( $L_c$ ), the rupture front accelerates rapidly and a “stick-slip” event is observed.



Results from Selvadurai and Glaser (2015, JGR)

## What is happening in the “seismogenic” section?

- Mature, unlubricated, rough-rough **frictional interface**
- Monitoring **localized seismicity** is a new development imparted by **improved AE sensors and techniques**.
- How is **localized seismicity** affected by:
  1. **Rupture front & speed ( $V_{prop}$ )**,
  2. **Loading velocity ( $V_{LP}$ )**,
  3. **Normal force ( $F_n$ )** and
  4. **Asperity distributions ( $b_{asp}$ )**
 is not well known.

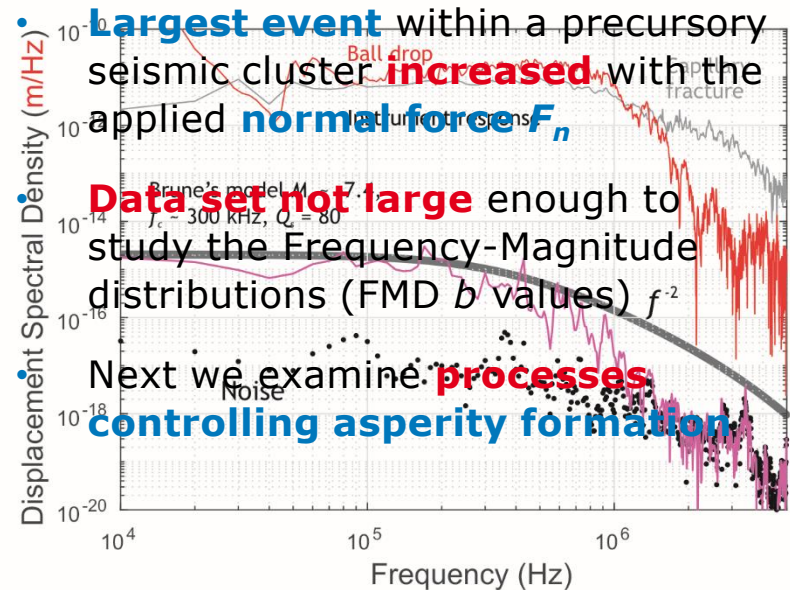
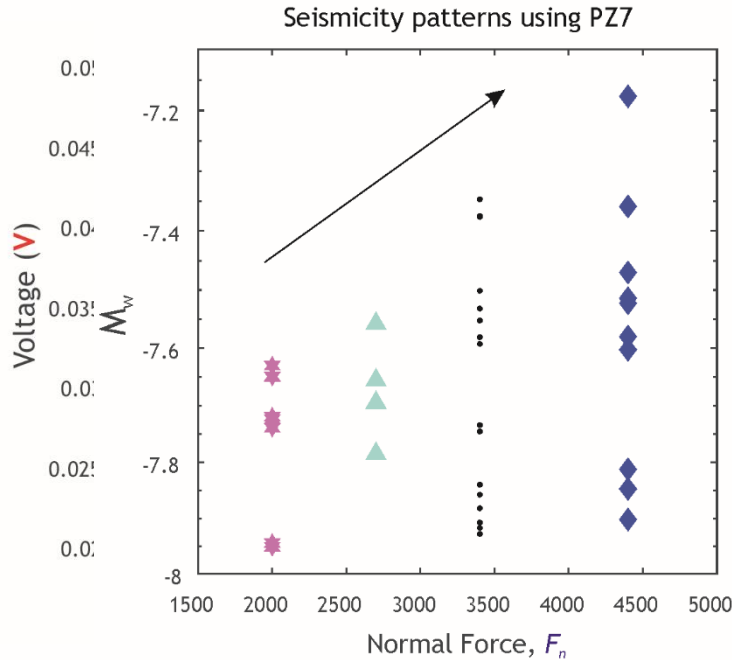


*"The best way to find a fault is to light them up with earthquakes"* – Dr. Gail Atkinson

**Experimental:** Goebel et al. (2012, 2013), McLaskey and Kilgore (2013), McLaskey et al. (2014), McLaskey and Lockner (2014), Passelègue et al. (2016), Selvadurai and Glaser (2015, 2017)

## AE sensor advances and localized seismicity patterns

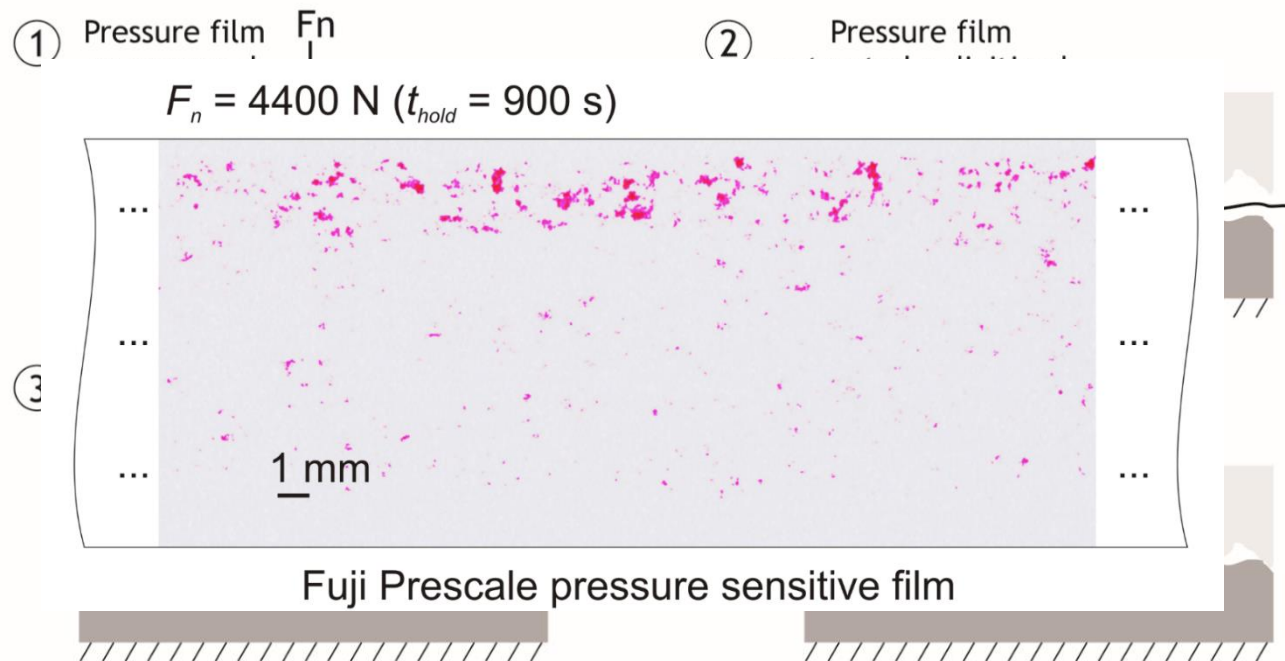
- AE sensor were absolutely calibrated → Frequency response in units [**m/Hz**]
- Precursory seismicity was located using **P-wave arrivals**
- Using **Brune's model** we estimate the **magnitude  $M_w$**



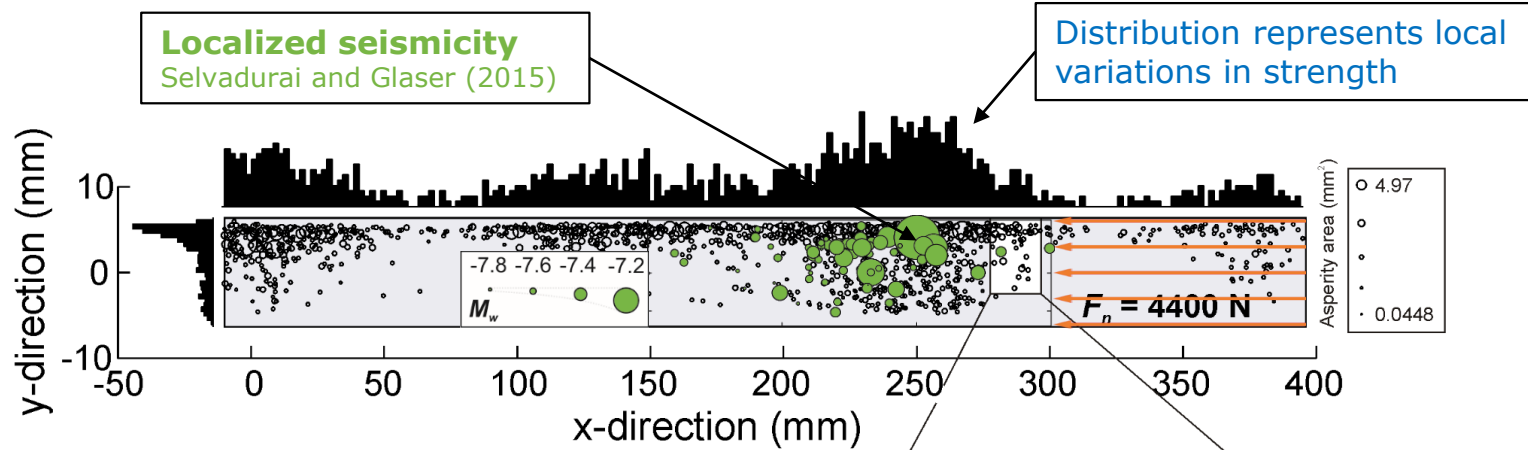


## Interface characterization:

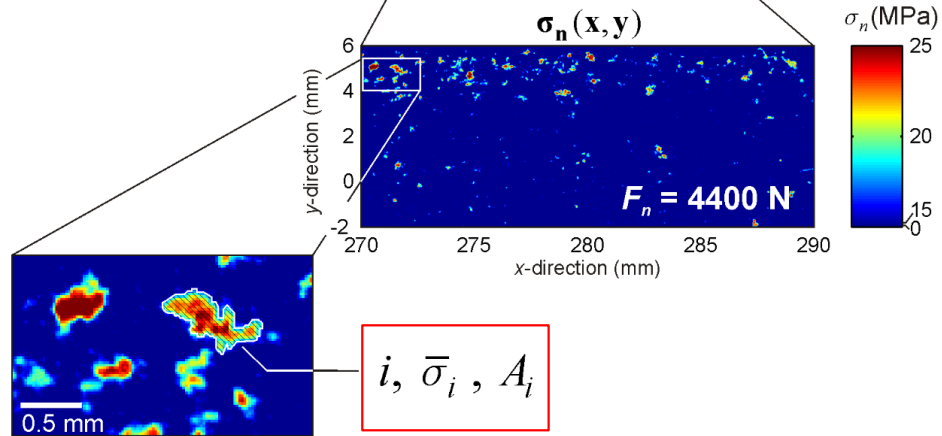
- Calibrated pressure sensitive film (FUJI Prescale Medium 12- 50 MPa)
- Compressed along interface, extracted and digitized.
- Provides *a priori* measurements of asperity distribution



# Asperity measurements



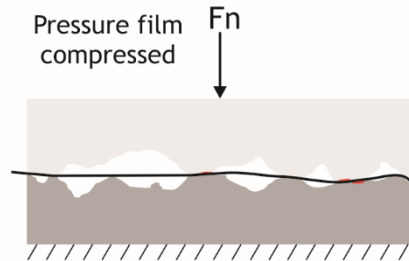
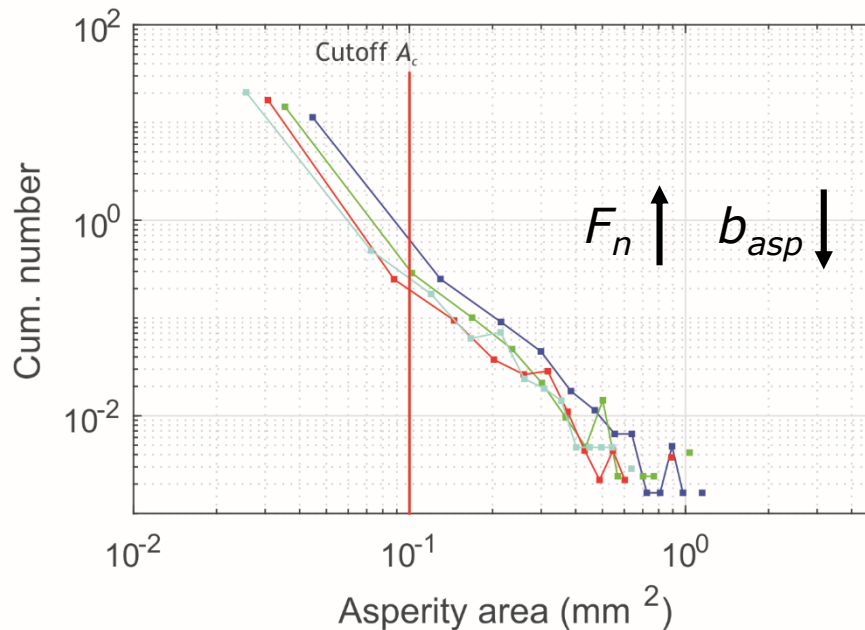
$i = i^{\text{th}}$  asperity  
 $\bar{\sigma}_i = \text{Mean normal stress (MPa)}$   
 $A_i = \text{Area (mm}^2\text{)}$



## Frequency-Asperity size distribution (FASD):

- We use a “pseudo”  $b$ -value ( $b_{asp}$ ) to describe asperity size distributions with changing normal loads in the seismogenic section of the fault

$$b_{asp} = \log_{10} \left( \frac{\sum_{i=1}^N A_i}{N A_c} \right) - \frac{A_{bin}}{2 A_c}$$

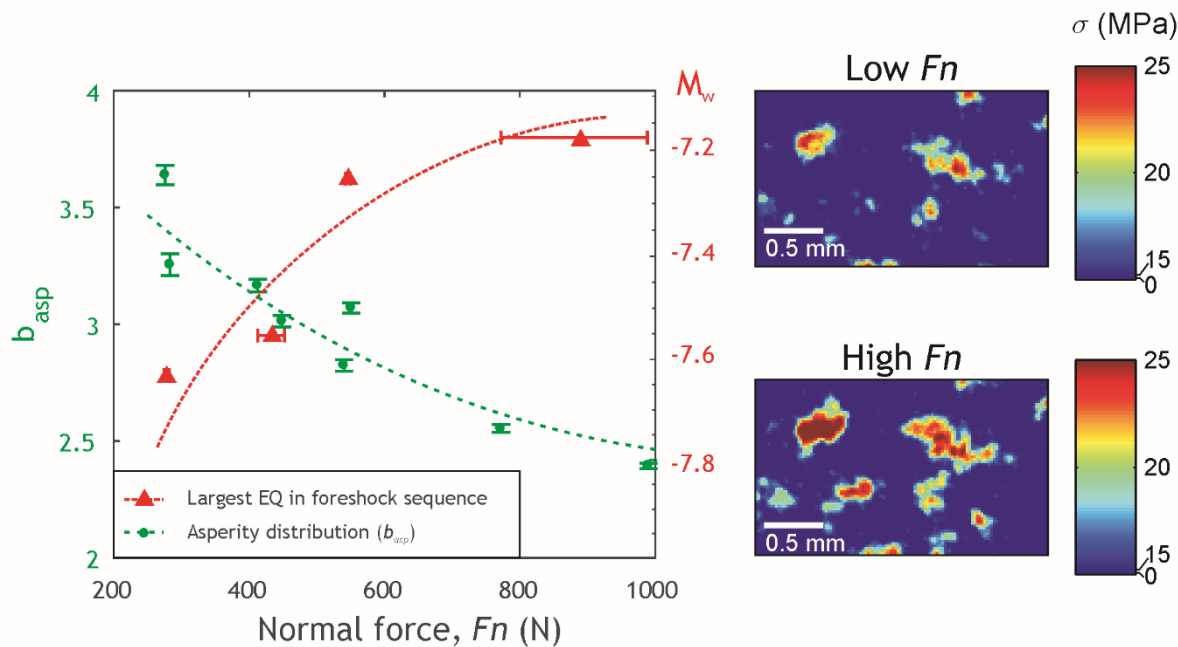


—■—	$b_{asp} = 2.3939$ , $N = 226$ , $F_n = 989.6 \text{ N}$
—■—	$b_{asp} = 2.8237$ , $N = 134$ , $F_n = 540.1 \text{ N}$
—■—	$b_{asp} = 3.0127$ , $N = 115$ , $F_n = 448.7 \text{ N}$
—■—	$b_{asp} = 3.6386$ , $N = 78$ , $F_n = 276.1 \text{ N}$

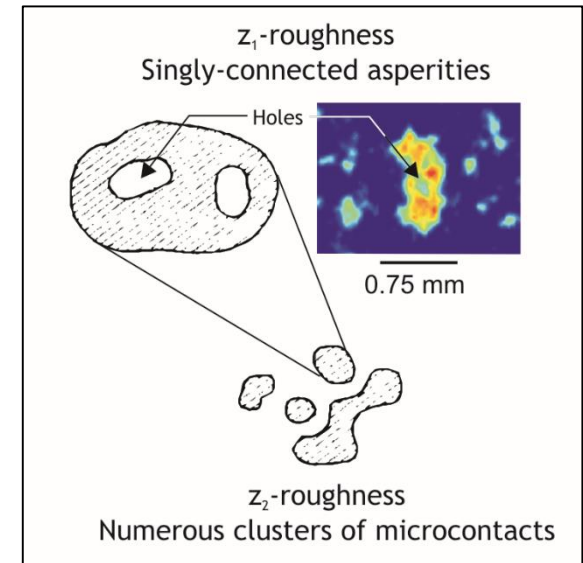
**Changes in  $b_{asp}$  should be related to contact processes and surface roughness**

## Asperity distributions versus normal load

- $b_{asp}$  decreased as  $F_n$  was increased
- Lower  $b_{asp}$  values indicate that the ratio of large to small asperities increased
- The potential for a large localized event may be linked to lower  $b_{asp}$  values

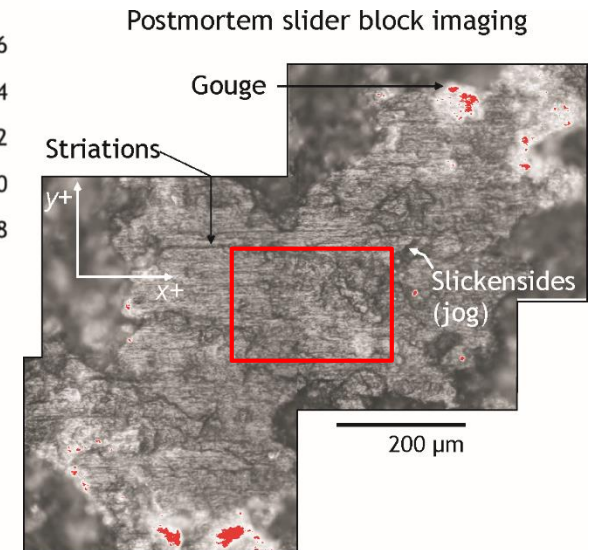
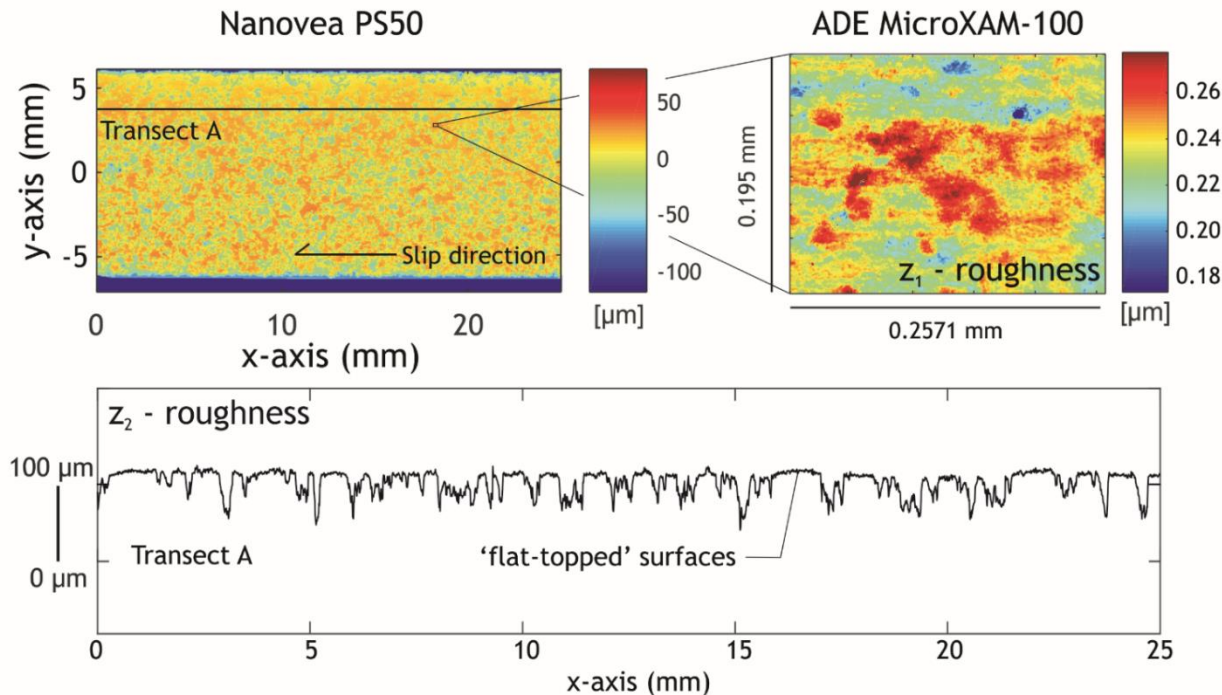


## Nayak's (1973) dominant wavelengths asperity model



## Asperity distributions related to mature roughness

- **Nayak's contact model** may explain how asperities formed in our tests based on **postmortem roughness** measurements of the slider block
- Dominant **longer** and **shorter** length scales in roughness



## Summary of findings

We performed a frictional study on a mature **PMMA-PMMA frictional fault** where the **normal load was varied** systematically

**Local precursor seismicity** ( $M_w \sim -7.1$  to  $-7.9$ ) was observed during the passage of a **slow nucleation front**

During foreshock sequences, **larger precursory seismicity** was present in sequences with **additional normal force**

This may **be linked to the manner in which asperities form** (measured using the pressure sensitive film)

Asperities formed due to **two dominant roughnesses** → could be linked to length scale dependent adhesive wear mechanisms\*

Thank you! Questions? [paul.selvadurai@sed.ethz.ch](mailto:paul.selvadurai@sed.ethz.ch)

- **Acknowledgements:**

- National Science Foundation Grant # 1131582 (S. Glaser)
- Jane Lewis Fellowship (P. Selvadurai)
- NSERC, PGS-Doctoral Fellowship (P. Selvadurai)
- Department of Defense Fellowship (J. Parker)

- **References:** <https://polybox.ethz.ch/index.php/s/AoqZK8R8fgoePPE>

